INVESTIGATION OF THE SUITABILITY OF PERIPHERAL LYMPHOCYTE MITOCHONDRIA AS AN INTRINSIC BIOLOGICAL DOSIMETER

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A Thesis

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by Charles E. Willis B.S., Louisiana State University, 1975 December, 1980

DEDICATION

This thesis is appropriately dedicated to my wife, Diana, who has always been committed to it. Her technical assistance in the isolation of the peripheral lymphocytes was as essential to the successful completion of this project, as was her continuous faith and encouragement. When I consider her contribution, I remember a young woman, several months pregnant, asleep on a pallet of lab coats, enjoying a brief respite from her long day of academics, her evening of work-study dishwashing, and her night of laboratory work on this project. The project is complete, but the memory lingers on.

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ABSTRACT

Using the human body as its own radiation dosimeter has attracted attention because the problem of questionable crossover functions is avoided. The possibility of using peripheral lymphocyte mitochondria as an indicator of radiation dose has not been examined previously, but has merit based on the chemiosmotic hypothesis of mitochondrial function. Swelling-response differences between damaged and undamaged mitochondria in irradiated specimens can be detected by a spectrophotometric method, which relates theoretically to the volume dependence of light scattering. Cobalt-60 gamma irradiated samples of isolated bovine peripheral lymphocyte mitochondria, exposed to doses from 2 to 275 rads, and control samples swelled under identical conditions yielded analytical data to test two theoretical models. The results do not allow unambiguous distinction between single-hit and multi-hit/multi-site hypotheses, but estimated target volumes by either hypothesis are near mitochondrial membrane volume. Probit analysis and empirical curve fitting lead to D₃₇ of approximately 170 rads. If it were possible to apply the results to human lymphocytes isolated post irradiation, the method would yield useful dosimetry between 2 and 250 rems.

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CHAPTER 1

INTRODUCTION

In order to better utilize nuclear technology, scientists and engineers must be able to measure radiation exposures accurately. Accurate measurements are of primary importance before it will be possible to assess both the short and long term physiological impact of radiation exposures.

There are three major shortcomings in the stateof-the-art for evaluation of personnel exposures. Exposures must be measured by some device; the device must be interpreted; and the interpreted measurement must be correlated to an expected biological effect.

First, our present system requires that the subject of radiation exposure wear on his person, or have in his proximity an appropriate radiation dosimetry device. More often than not, the subject is either not wearing his dosimeter or does not have easy assess to one. Dosage in this case is usually estimated by field measurements or calculations before or after the exposure event.

Second, the matter of interpretation of the properly worn dosimeter is a matter of some ambiguity because of the physical characteristics of the particular device, the spatial distribution of the radiation dose, location of the dosimeter, and temporal distribution of dose.

Third, the response of a given dosimeter may or may not be correlated to any real biological response to radiation exposure. For example, the Relative Biological Effectiveness (RBE) is a correction factor introduced into the dose calculation to adjust values obtained through physical dosimetry to approximate some particular observed biological response. There is still controversy over whether there is a threshold for radiation damage in humans, which is associated with statistical interpretation of largely non-existent data (Fremlin, 1980; Land, 1980). Some measurable doses of radiation cause no detectable biological effects, and some effects manifest themselves in the apparent absence of detectable radiation dose above background. The choice of the biological effect to be monitored is likewise no simple matter since there is still no consensus of opinion as to the specific primary site of radiation damage in living organisms.

With the ultimate aim of obviating the inherent deficiencies of physical dosimetry, the purpose of this thesis is to investigate the feasibility of the use of lymphocyte mitochondria as a limiting indicator of radiation dose to the whole organism.

CHAPTER 2

CRITERIA FOR SELECTION OF AN INTRINSIC BIOLOGICAL DOSIMETER

Theoretically, all three problems introduced in Chapter 1 can be circumvented by the use of an intrinsic biological dosimeter, that is, some organ or structure, common to all members of a species, which will manifest some detectable response to the absorption of energy from a radiation field. In the most idealistic case, this dosimeter would be easily extractable in its native state, with little or no concommittant harm to the donor organism; would be sensitive enough to radiation to measure small doses, especially prior to the onset of the acute physiological syndromes; and would lend itself to study in the extracted state. If the structure in question is not, itself, the primary site of radiation damage, it should at least share functional characteristics with other structures of the body, and be well enough dispersed to provide random sampling and a representative picture of the remainder of the organism. The selection of a candidate tissue for radiobiological dosimetry is not a simple matter, and requires some knowledge of the differential response of human tissues to radiation.

Selection of a Radiosensitive Tissue

The attribute of relative "radiosensitivity" has meaning for comparison of two tissues only when qualified by the criterion used to evaluate sensitivity. Based on the criterion of "early cell death", defined as death before a given number of mitotic cycles;

Mature lymphocytes (one of the two major classes of circulating white blood cells), erythroblasts (red blood cell precursors), and certain of the spermatogonia (most primitive cell in the spermatogenic series) are undoubtedly the most radiosensitive mammalian cells. (Casarett, pp. 168-169)

Of these, both the erythroblasts and spermatogonia are localized, and although each has been proposed as a biological dosimeter (Segreto, et al., 1974; Ceraci, et al. 1974), neither are convenient because of the difficulties involved in sampling and the calculation of the spatial dose distribution. The mature lymphocytes are, on the other hand, freely circulating which would afford random sampling. Furthermore, lymphocytes are rather undifferentiated, as evidenced by their ability to survive and function in vitro, which implies that they should reflect the general characteristics of other cells. Casarett (p. 178) has reported that lymphocytes are sensitive to acute whole body exposures as low as 10 R. Earlier work with lymphocytes was restricted to cultured cells, by technical difficulties with quantitative isolation (Davis, 1967).

Lymphocytes have been studied extensively for the purpose of dosimetry with various damage indicators (Tamura and Sugiyama, 1974; Silberstein, <u>et al</u>., 1974; Madhvanath, 1976). These studies were done with cultured lymphocytes, which subjects the cells to a selection process, and can lead to misinterpretation of the results. The functional properties of cultured cells are notably different from those in the native state (Elkind and Whitmore, 1967; p. 154, Casarett). There are now a variety of techniques available for the extraction of pure, viable lymphocytes from relatively small samples of peripheral blood, and these methods were reviewed by Willis (unpublished, included in part as Appendix A).

Selection of the Manifestation of Radiation Damage

Regardless of which radiosensitive cells are selected, it is necessary to choose a particular physiological manifestation of radiation damage to be monitored. Historically, one of the first attempts to quantitate radiation exposure was the Skin Erythema Dose (SED), which was defined as that amount of radiation required to produce reddening of human skin within 1 to 2 weeks. The results of this method were not known until three weeks after the exposure, and the variability among subjects, was considerable. Skin reddening is not uniquely associated with radiation exposure, nor is it representative of the internal damage caused by the dose.

The occurrence and viability of lymphocytes has been used (Madhvanath, 1976) as an indicator of radiation damage, however the attenuation of the lymphocyte population in itself bears little information as to the generalized damage to other tissues. An intelligent choice of the biochemical indicator of radiation damage requires knowledge about the cellular response to radiation and understanding of theories about the primary site of radiation damage.

Theoretical Biological Lesions Caused By Radiation

Disturbances in metabolism are the most obvious effects of radiation at the physiological level. These disturbances are not confined to radiation effects, but also occur in natural pathological conditions. The first attempt to explain such physiological effects at the cellular level was the Enzyme Release Hypothesis (pp. 272-277, Bacq and Alexander), which proposed that the membranes of lysosomes were damaged by radiation, leading to the release of degradive enzymes and toxic substances that could cause the destruction of the cell. Later, when it was found that doses greater than 100 rads were necessary to produce detectable leakage of the lysosomal contents, this hypothesis was modified to suggest, instead, a physical disturbance of the spatial arrangement of the enzymes of the respiratory chain (v.i.). With aspersions

now cast on the Enzyme Release Hypothesis, the dominant theory became the Nuclear Damage Hypothesis (Coggle, 1971).

For many years it was known that ionizing radiation induced structural aberrations in chromosomes (Casarett, pp. 99-113) at doses of less than 10 rad (pp. 81-113, Coggle). In fact, H. J. Muller was awarded a Nobel Prize for demonstrating the induction of lethal mutations on Drosophilla chromosomes by the use of X-rays. Most of the work in the field of biological dosimetry has been directed toward determination of the dose-versus-chromosomalaberration response function (Madhvanath, 1976). However, the usual cellular consequence of a chromosomal aberration is death during that particular mitotic cycle, or growth without cell division so that this gross manifestation is a poor rationale for the heritible changes produced by radiation. More subtle damage to chromosomal DNA is presumed to be the source of these mutations. Subtle damage should be reparable by one of several mechanisms now known to exist within the nucleus (Dugle, et al., 1976). Since it has been well established that a high percentage of random mutations are lethal (Rees, 1967), there is a statistical bias against residual damage being passed on to subsequent generations. If it is, heterozygosity often masks its expression in the adult. A contemporary version of the Nuclear Damage Hypothesis assumes damage to DNA repair mechanisms (Witkins, 1969).

From a chemical-physical perspective, the primary site of radiation damage is the cell's own water content. Radiation is known to generate free radicals in aquaeous solutions, and some degree of radiation protection is afforded by substances having free radical scavenging abilities. Free radicals are highly reactive chemical species and can propagate not only through water, but also through most biomolecules, and can directly interfere with some enzyme reactions (pp. 375-376, Bacq and Alexander). Free radical reactions in the cell result in additional production of toxic peroxides, which, however, can be removed by catalase.

The enzyme interference phenomenon is only observed during irradiation, which eliminates the possibility of direct dosimetry by this process because there is no stored information for post-irradiation recovery. Residual damage to a sensitive biological structure must still be identified to make use of this chemical information. Bacq and Alexander have identified two candidates with known sensitivity to free radicals: DNA; and sulfur-containing enzymes (Ibid, p. 328), most of which are located in the mitochondria.

There is general agreement that the mechanism of radiation damage in cells is not a discrete phenomenon, but a collection of effects on different cell structures.

However, there is a growing volume of evidence that the primary observed effects of radiation may be traced to multiple forms of damage to the cell's mitochondria (Coggle, 1971).

Mitochondria are small organelles with double membranes, occurring in all mammalian cells in numbers which vary from several to several thousands. Mitochondria contain their own DNA which replicates on a time schedule independent of the nuclear mitotic event. This attribute gives them interesting genetic significance (Fine, 1978; also p. 3, Appendix B). The mitochondrion's primary function is the production of high energy compounds (ATP) for utilization in most other cell processes. The production of ATP by oxidative phosphorylation depends on the integrity of the inner mitochondrial membrane, across which a proton (H⁺) gradient (Mitchell, 1979) is developed and maintained by the mechanisms of an electron transport This gradient provides the driving force for the chain. production of ATP. One of the notable characteristics of radiation is that it uncouples the process of electron transport from the process of oxidative phosphorylation with exposures as little as 25-100 R (p. 331, Bacq and Alexander). The mode of action of other uncouplers is to cause the collapse of the proton gradient (p. 519, Lehninger). It is clear that a lesion (or hole) in the inner membrane caused by the action of radiation could

permit free passage of protons, which would result in the cessation of ATP production and an increase in ATP breakdown. The idea of a biochemical lesion to the inner mitochondrial membrane is a further modification of the Enzyme Release Hypothesis in that it incorporates aspects of both free radical chemical damage to biomolecules (Orlov, <u>et al.</u>, 1976; Mustea, <u>et al.</u>, 1978; Nohl and Hegner, 1978a, 1978b) and genetic consequences of radiation damage (von Wagenheim, 1976).

Selection of Damage Criteria

The application of mitochondria damage to radiation dosimetry requires quantitation of the damage, either by direct observation of separated cells, by observation of some change in cellular behavior, or by an altered property of the mitochondria themselves. Morphological changes in mitochondria are the earliest manifestations of radiation damage detectable by electron microscope (Goldfeder and Selig, 1969; Cottier, <u>et al</u>., 1963). Another direct microscopic observation of mitochondrial damage is "cloudy swelling," which is considered indicative of some disruptive cytological influence.

Mitochondria can be isolated and studied from several aspects. Activity of the enzyme malate dehydrogenase, normally retained inside the intact mitochondrion, is released if the organelle is damaged. The capacity of

isolated mitochondria to produce ATP can be measured by means of an oxygen polarigraph (Chance and Williams, 1955; Reed, 1972).

Two conformations of isolated mitochondria have been observed by both electron microscopy, and by isopycnic density gradient centrifugation (Beaufay, <u>et al</u>., 1964; Murfitt, <u>et al</u>., 1978; Holtzman, <u>et al</u>., 1978; Lemasters, 1978), as illustrated in Figure 1. The orthodox configuration is indicative of normal, energized, osmotically active mitochondria. The condensed configuration is associated with abnormal states, such as osmotic shock and myocardial infarction, and is deenergized and osmotically inactive.

Another interesting ability of the mitochondrion is to undergo large volume changes, called "mitochondrial swelling," which are observed both <u>in vivo</u> and in isolates. The presence, duration, and degree of mitochondrial swelling has been used as an indicator of damage in a variety of normal and pathological conditions (Mihai, <u>et al</u>., 1973; Chen and Chang, 1978; Fowler and Woods, 1977; Porter, <u>et al</u>., 1979). There is a significant difference between <u>in vivo</u> and <u>in vitro</u> swelling. As mentioned above, swelling observed <u>in vivo</u> is a phenomenon of nonspecific origin. <u>In vitro</u> swelling, on the other hand, is a demonstration of the mitochondrial response to its biochemical environment.



STICE.



Configuration	ORTHODOX	CONDENSED
Associated metabolic state	Energized	Deenergized
Outer compartment oncotic pressure	High	Low
Osmotic pressure gradient	High	Low
Assumed structural state	Normal	Damaged

Figure 1. Two Conformations of Mitochondria (after Lemasters, 1978).

The three classes of <u>in vitro</u> swelling are: osmotic swelling; energy-linked swelling; and transportrelated swelling (Harman and O'Hegarty, 1962; Lehninger, 1962; Packer, 1963). Osmotic swelling is caused by the uptake of water in order to satisfy a concentration gradient resulting from the rapid dilution of the mitochondria into a medium much lower in the concentrations of certain internal solutes, such as sucrose, which have a limited permeability. Energy-linked swelling is an increase in volume which accompanies the active process of oxidative phosphorylation. Volume changes are also associated with the active transport of metabolites across the membrane (Harris, 1972).

From a theoretical viewpoint, osmotic swelling is the simplest of the three swelling phenomena to describe. Swelling also offers direct observation of the dynamic behavior of isolated mitochondria, and therefore has the best possibility for success in the evaluation of mitochondria as an intrinsic biological dosimeter.

CHAPTER 3

THEORETICAL TREATMENT OF TURBIDOMETRIC MEASUREMENTS

On the basis of the foregoing development, lymphocyte mitochondria appear to be the best candidate for an intrinsic biological dosimeter, and osmotic swelling appears to be the most straightforward process to quantify damage. Theoretical details of the application of swelling measurements for dosimetric purposes are examined in the ensuing paragraphs.

Mitochondrial swelling was first observed in vitro in teased preparations by Koelliker (1888) using a light microscope. Since then, a variety of methods have been applied to the study of mitochondrial volume changes, including phase contrast microscopy (Pauly, et al., 1960; Pauly and Packer, 1960), electron microscopy (Malamed, 1965), electronic particle sizing (Gebicki and Hunter, 1964), radioactive tracers (Tarr and Gamble, 1966), and light scattering/nephelometry (Latimer, 1979). By far the most commonly-used method is turbidometric measurement, by means of absorbance changes on a spectrophotometer. These absorbance changes are a result of light scatter caused by the difference in refractive index between the solution and the interior of the organelle (Wallach, et al., 1966; Oster, 1948; Duniec and Thorne, 1977). An important

analytical treatment of osmotic changes in mitochondrial volume with respect to sucrose penetrability was conceived by Tedeshi (1965). The classical treatment of the relationship between absorbance and volume changes was by Koch (1961). In order to examine the osmotic response of mitochondria, it is necessary to describe the phenomena of swelling and light scatter changes more generally.

Simple First Order Approximation

By a purely thermodynamic argument for conditions of constant temperature, pressure, mass, etc., under which swelling occurs, one would expect the swelling process to exhibit first order kinetics. This presumes that once initiated, osmotic swelling depends on time as the only independent variable. Without detailed knowledge of the process, it is possible to suggest a simple diffusionrate model, in which the rate of swelling, d(V(t))/dt, at any time, t, is proportional to the difference between the attainable volume, V_s . The maximum volume will be reached when the gradient driving forces are resolved. Mathematically,

$$\frac{d[V(t)]}{dt} = L[V_{s} - V(t)], \qquad (3.1)$$

in which L is a constant of proportionality. An
analytical solution of equation (3.1) for the function
V(t) can be obtained as follows:

$$\frac{d[V(t)]}{dt} = y' = LV_s - Ly , \qquad (3.1a)$$
$$V_s L = y' + Ly ,$$

$$V_{s}Le^{Lt} = y'e^{Lt} + Le^{Lt}y . \qquad (3.2)$$

Using the Product Rule, when L is constant,

$$d[ye^{Lt}] = y'dt \cdot e^{Lt} + Le^{Lt}dt \cdot y;$$

Or,

$$\frac{d[ye^{Lt}]}{dt} = y'e^{Lt} + Le^{Lt}y . \qquad (3.3)$$

Then, substituting equation (3.3) into equation (3.2):

$$V_{s}Le^{Lt} = \frac{d[ye^{Lt}]}{dt},$$

$$V_{s}Le^{Lt}dt = d[ye^{Lt}].$$
(3.4)

Integration of equation (3.4), with V_0 as the constant of integration yields:

t
$$V_{s}Le^{Lt}dt = ye^{Lt}$$
o

$$ye^{Lt} = V_{s}e^{Lt} + V_{o}. \qquad (3.5)$$

But

$$y = V(t) ;$$

$$V(t)e^{Lt} = V_{s}(e^{Lt} - 1) + V_{o} ,$$

$$V(t) = V_{s}(1 - e^{-Lt}) + V_{o}e^{-Lt} ,$$

$$V(t) = V_{s} - V_{s}e^{-Lt} + V_{o}e^{-Lt} ,$$

$$V(t) = V_{s} - (V_{s} - V_{o})e^{-Lt} .$$
(3.6)

If a new parameter for the volume change, ${\tt V}_{\rm c},$ is defined such that

$$V_c = V_s - V_o$$
,

then equation (3.6) becomes

$$V(t) = V_{s} - V_{c}e^{-Lt}$$
 (3.7)

The form of equation (3.7) is that of a typical saturation function. By this approximation, the volume of the mitochondrion increases rapidly at the onset of swelling, and assymptotically approaches a maximum value,

 V_s . The rate of expansion is governed by a first order rate constant, L, and two constant coefficients, V_s and V_c .

Application of Fick's Law of Diffusion

Equation (3.7) is based on no knowledge of the mechanism of swelling. An alternate approach to the mathematical description utilizing Fick's Second Law of Diffusion has been proposed by Tedeshi (1965). This approach takes into account the fact that the rate of influx depends on the surface area available for diffusion, as well as time.

Tedeshi's statement of Fick's Law is as follows:

$$\frac{dC_{i}(t)}{dt} = k \frac{A(t)}{V(t)} [C_{0} - C_{i}(t)]$$
(3.8)

in which $C_i(t)$ is the internal concentration of some solute, k is the permeability constant, A(t) is the surface area subject to diffusion of solute, V(t) is the volume, and C_0 is the external concentration of solute. A special case for equation (3.8) is apparent when water is the permeable molecule and C_0 is constant by virtue of an overwhelming concentration which changes little during the swelling process. For this case, when M is the mass of impermeable solute,

$$C(t) = M/V(t)$$
 (3.9)

Use of this relationship in equation (3.8) yields

$$\frac{d\left[\frac{M_{i}}{V(t)}\right]}{dt} = k \frac{A(t)}{V(t)} \frac{M_{o}}{V_{o}} - \frac{M_{i}}{V(t)} , \qquad (3.10)$$

in which the subscripts i and o refer, respectively, to internal and external quantities. For simplicity, equation (3.10) and all subsequent equations will be written without specific designation of time-dependent variables:

$$\frac{d(M_i/V)}{dt} = k(A/V) \left(\frac{M_o}{V_o} - \frac{M_i}{V}\right) . \qquad (3.10a)$$

Because the impermeable solute mass remains constant,

$${}^{M}_{i} \frac{d(1/V)}{dt} = k \frac{A}{V} \left(\frac{M_{o}}{V_{o}} - \frac{M_{i}}{V}\right) ;$$

$$\frac{d(1/V)}{dt} = k \frac{A}{V} \left(\frac{M_{o}}{V_{o}M_{i}} - \frac{1}{V}\right) . \qquad (3.11)$$

Rewriting,

$$d(1/V) = d(V)^{-1} = -(V)^{-2} dV = -dV/(V^{2}) ,$$

$$-\frac{1}{V^{2}} \frac{dV}{dt} = k \frac{A}{V} \left(\frac{M_{o}}{V_{o}M_{i}} - \frac{1}{V} \right) ,$$

$$-\frac{dV}{dt} = k \frac{A}{V} \left(\frac{M_{o}V}{V_{o}M_{i}} - 1 \right) . \qquad (3.12)$$

In a sucrose solution, mitochondria assume a nearly spherical shape (Pauly, <u>et al</u>., 1960); hence, the surface area and volume are functions of the time-dependent radius, r:

$$A = 4\pi r^2$$
; (3.13a)

$$V = \frac{4}{3}\pi r^3 .$$
 (3.13b)

Substitution of these relations into equation (3.12), and rearranging, results in an expression for the swelling rate, as represented by the change of the radius with time:

$$-\frac{d(\frac{4}{3}\pi r^{3})}{dt} = k \frac{4\pi r^{2}}{\frac{4}{3}\pi r^{3}} \left(\frac{M_{0}4\pi r^{3}}{3V_{0}M_{1}} - 1\right) . \qquad (3.14)$$

Dividing $4\pi/3$ into both sides gives

$$-\frac{dr^{3}}{dt} = k \frac{3}{r} \left(\frac{M_{o}r^{3}}{V_{o}M_{i}} - \frac{3}{4\pi} \right) ; \qquad (3.15)$$

$$-\frac{dr^{3}}{dt} = k \frac{9}{4\pi r} \left(\frac{4\pi r^{3}M_{0}}{3V_{0}M_{i}} - 1\right) . \qquad (3.15a)$$

Recognition that $dr^3 = 3r^2 dr$, and substitution into equation (3.15a) results in:

$$-3r^{2} \frac{dr}{dt} = k \frac{9}{4\pi r} \left(\frac{4\pi r^{3}M_{o}}{3V_{o}M_{i}} - 1\right) ,$$

which may be simplified to

$$\frac{dr}{dt} = -\frac{3k}{4\pi r^3} \left(\frac{4\pi r^3 M_0}{3V_0 M_1} - 1 \right)$$

Finally,

$$\frac{dr}{dt} = \frac{3k}{4\pi r^3} - \frac{kM_0}{V_0M_i} .$$
 (3.16)

Making use of the volume formula again and the definition of concentration (see equation 3.8):

$$\frac{\mathrm{d}\mathbf{r}}{\mathrm{d}\mathbf{t}} = \frac{\mathbf{k}}{\nabla} - \frac{\mathbf{k}C_{0}}{M_{i}} \qquad (3.17)$$

Definition of K_2 as an appropriate constant coefficient reveals the form of equation (3.17):

$$\frac{\mathrm{d}\mathbf{r}}{\mathrm{d}\mathbf{t}} = \frac{\mathrm{k}}{\mathrm{V}} - \mathrm{K}_2 \quad . \tag{3.18}$$

At equilibrium dr/dt = 0; hence,

$$0 = \frac{K}{Veq} - K_2,$$

$$K_2 = \frac{K}{Veq},$$

$$Veq = \frac{K}{K^2} = \frac{K}{C_0/M_1},$$
(3.19)

or, simply,

$$Veq = \frac{M_i}{C_o}$$
. (3.20)

The value of equation (3.19) is constant for the assumed conditions of C_o and M_i. Substitution of equation (3.19) back into equation (3.18) results in

$$\frac{\mathrm{dr}}{\mathrm{dt}} = \frac{\mathrm{k}}{\mathrm{V}} - \frac{\mathrm{k}}{\mathrm{Veq}}$$

or,

$$\frac{\mathrm{d}\mathbf{r}}{\mathrm{d}\mathbf{t}} = \mathbf{k} \left(\frac{1}{\mathbf{V}} - \frac{1}{\mathrm{Veg}}\right) \quad . \tag{3.21}$$

There is a striking similarity between equation (3.21) and equation (3.1). The difference is, however, significant enough to prevent analytical solution by the same method as equation (3.1). Equation (3.21) can be rewritten in the following form:

$$\frac{dr}{dt} = \frac{a}{r^3} - b$$
, (3.22)

in which $a = 3k/4\pi$ and b = k/Veq. After determination of a common denominator, and rearrangement,

$$\frac{\mathrm{dr}}{\mathrm{dt}} = \frac{\mathrm{a} - \mathrm{br}^3}{\mathrm{r}^3}$$

integration becomes possible

$$\frac{r^3 dr}{(a - br^3)} = dt = t + c$$

which is a form consistent with the equation 86, page 410, CRC Standard Math Tables (Selby, 1969). The solution is:

$$t + c = \frac{1}{b} dr - \frac{a}{b} \frac{dr}{(a + br^3)}$$
 (3.23)

The first term of equation (3.23) can be solved and the second term can be replaced with the analytical solution given by equation 74, (Ibid. page 409). This yields:

$$t + c = \frac{1}{b} (r - r_{o})$$

$$- \frac{a}{b} + \frac{h}{3a} \left[\frac{1}{2} \log \frac{(h + r)^{3}}{a + br^{3}} + 3 \tan^{-1} \frac{2r - h}{h - 3}\right]$$

 $h = 3 \frac{a}{h}$

in which

Modification for the Effects of Surface Tension

Volume change in a mitochondrion is resisted by surface tension (Racker, 1970), elastic forces within the membrane (Trudell, 1977), or damping of the osmotic gradient by the outer membrane (Lemasters, 1978). This requires the modification of the rate equation (3.22) to account for resistance to expansion. The usual way to correct rate equations for the effects of surface tension is to

(3.24)

subtract a term for the resistance. This results in an equation of the following form:

$$\frac{dr}{dt} = \frac{\alpha_1}{r^3} - Kr - \alpha_2 , \qquad (3.25)$$

in which K is the membrane's constant of elasticity, and a_1 and a_2 are constants. The middle term implies that the resistance increases linearly with the radius. There is no analytical solution available for equation (3.23). Nevertheless, using a fourth-order Runge-Kutta approximation (Conte, pp. 336-339), it is possible to get a good approximation of r(t) with errors of h^5 (e.g., data taken each 0.5 minutes during a ten-minute assay will yield 3.125×10^{-7} min-error/min).

Probabilistic Model of Light Scatter

As opposed to light scattering methodology, turbidometric measurements have the advantage of avoiding the assumption of an angular distribution function for scattered light. The following treatment describes reduction in light intensity by suspended mitochondria, including both light scatter and absorption. The specific discussion of energy absorption is not included here, but the approach utilized may also find application for description of energy deposition in mitochondrial membranes. Assuming a spherical mitochondrion (see Figure 2), the radius increases as the following function of volume (Malamed, 1965):

$$r = \left(\frac{3V}{4\pi}\right)^{1/3}$$
 (3.26)

Correlative assumptions are that the membranes form a spherical shell about the mitochondrion (Wallach, <u>et al.</u>, 1966), and that the shell thickness, a, is small compared to the radius, r (actually, a/r = 1/100; Racker, page 21). The volume of the shell is then given by:

$$V_{\text{shell}} = 4\pi r^2 a \qquad (3.27)$$

Further necessary assumptions are that the total amount of material making up the membrane is constant (no protein or lipid assimilation, fixation, or association over the 10 minute test), and that the density of the material does not change:

if: dMass = 0 ;
and: dDensity = 0 ;
then: dV_{shell} = 0 . (3.28)



Although the density assumption may appear trivial, the consequence is to allow the quantity "a" to embody all of the membrane structural characteristics, including thickness and conformation (density and compactness). It should be noted that decreases in membrane thickness during swelling have been reported in the literature (Trudell, 1977).

Differentiating equation (3.27) by means of the Product Rule:

$$dV_{shell} = a 8\pi r dr + 4\pi r^2 da$$
.

Then, by the use of equation (3.28);

$$dV_{shell} = a 8\pi r dr + 4\pi r^2 da = 0 ;$$

$$4\pi r^2 da = -a 8\pi r dr$$

or,

$$\frac{\mathrm{da}}{\mathrm{a}} = -\frac{8\pi r \mathrm{d}r}{4\pi r^2} ,$$

$$\frac{\mathrm{da}}{\mathrm{a}} = -\frac{2}{\mathrm{d}r} . \qquad (3.29)$$

Integrating equation (3.29) yields:

$$\ln(a) \alpha - 2[\ln(r)];$$
and, by exponentiation

$$a \alpha \frac{1}{r^2}$$
 (3.30)

Since the swelling is monitored by a spectrophotometer, the change in "thickness", da, of the membrane is critical to the light transmission characteristics of the mitochondrion. If μ_{ℓ} (Mu) is the linear attenuation coefficient for the mitochondrion, then we can express μ_{ℓ} as:

$$\mu_{o} = \sigma_{T} A_{eff} \qquad (3.31)$$

in which $\sigma_{\rm T}$ is the total microscopic probability for any interaction which would prevent the transmission of light into the sensitive volume of the phototube detector, and $A_{\rm eff}$ is the effective area of the target mitochondrion. Since the mitochondrion is assumed to be spherical, the effective area is proportional to the cross-sectional area (Malamed, 1965):

$$A_{eff \alpha \pi r^2}$$
(3.32)

The interaction probability, σ_{T} , is a function of the density of the material which must be traversed by the light,

$$\sigma_{T} = f(surface density)$$

in which

surface density =
$$\frac{a(\text{thickness}) \times \text{Mass}(\text{gm})}{4\pi r^2}$$
(surface area).

Since the amount of material in the membranes is constant:

$$\sigma_{\rm T} \propto \frac{a}{\pi r^2}$$
(3.33)

Substituting equations (3.32) and (3.33) into equation (3.31):

$$\mu_{l} \propto \left(\frac{a}{\pi r^{2}}\right) (\pi r^{2})$$
,

or,

$$\mu_{l} \alpha a$$
 (3.34)

Combining equations (3.30) and (3.34) leads to the following relationship between the linear attenuation coefficient and the radius:

$$\mu_{l} \alpha r^{-2}$$
 (3.35)

As is conventional for beam attenuation theory (see Glasstone, p. 69), the total macroscopic attenuation

is equal to the sum of the individual microscopic attenuations:

$$\Sigma_{l} = p \sum_{i=1}^{N} r_{i}^{-2};$$
 (3.36)

in which Σ_{l} is the linear macroscopic attenuation coefficient, p is a proportionality constant (which can be adjusted to unity by selection of arbitrary units of radius), r_{i} is the radius of the ith mitochondrion, and N is the total number of mitochondria in the beam path. It should be noted that this treatment in terms of collision cross-section is, in principle, similar to Mie scattering theory (page 329, Oster; Koch, 1961).

Transmission Characteristics of a Heterogeneous Solution of Mitochondria

One can imagine the possibility of the existance of several discrete groups of mitochondria, which have similar swelling characteristics (Tedeshi, 1965; Willis, unpublished, included in part as Appendix B). This being the case, it is straightforward to write equation (3.36) as

$$\Sigma_{\ell} = p \sum_{i=1}^{N} P_{i}r_{i}^{-2} . \qquad (3.37)$$

in which P_i is the relative abundance of the ith group of n groups of mitochondria.

The transmission of light as measured by a spectrophotometer is given by the Lambert-Beer relation for uncollided flux, which is, in our case,

$$T = \frac{I}{I_0} = e^{-\sum_{\ell} X}$$

in which x is the beam path length; Σ_{g} is the macroscopic linear attenuation coefficient, or turbidity, τ (Oster, page 322); and T is the fractional transmittance, which is defined as the ratio of the observed intensity, I, to the incident intensity, I_{o} .

Substitution of equation (3.37) into the Lambert-Beer relation yields

$$T(t) = e \quad i=1 \quad (3.38)$$

With unit path length and arbitrary units of r such that p = 1, the following model for the time dependent transmittance is obtained from equation (3.38):

$$T(t) = e i=1$$
 $P_{i}r_{i}^{-2}$ (3.39)

Equivalently, in terms of volume,

$$T(t) = e^{\sum_{i=1}^{N} P_i V_i}$$
(3.39a)

This treatment is an important restatement of scattering theory for large particles, namely, that as the particle radius increases, the scattering out of the system will decrease (page 333, Oster). This conclusion is neither based on the assumption of an angular scattering distribution function, nor on the fallacious assumption that a decrease in the number of particles in solution per unit volume will occur with an increase in particle radius, as is the current explanation of large particle scatter (page 333, Oster). Nonetheless, the result bears a striking similarity to the result of the classical treatment by Koch (1961; eq. 11, p. 454).

Limitations of the Mathematical Model

The model assumes only osmotically generated swelling. Other modes of swelling may occur simultaneously in the reaction mixture, resulting in distortion of the shape of the swelling curves, as indicated schematically in Figure 3. The consequence of such interference would be the failure of the computer program to properly fit the data, or the imprecise determination of rate constants. Since transport processes have typically fast rates (Harris, 1972) and since oxidative phosphorylation is at a minimum (only endogenous substrates are available to the mitochondria), these interferences are probably minimal.

Another source of interference could come from contamination of the solution by osmotically active



microsomes (Tedeshi, <u>et al</u>., 1963; Wallach, <u>et al</u>., 1966; see also Appendix B). These would contribute to the overall transmittance change observed. The model would account for such contaminants by the inclusion of an appropriate swelling group or groups.

The model does not account for the possibility of fragmentation during the progress of swelling. It is possible to calculate the degree of this process (v.i.). The model can account for a low occurence of intact mitochondria at the onset of swelling through the parameter, P_i .

The final limitation is the source of mitochondria for application of the method. If the radiation dose has been high enough to substantially attenuate the number of peripheral lymphocytes, blood sample size will have to increase proportionately to yield enough mitochondria to produce detectable changes on the spectrophotometer. However, if the radiation dose is high enough to severely reduce the number of circulating lymphocytes, it is already standard techniques.

CHAPTER 4 DOSIMETRIC QUANTITATION

Three preceeding chapters have explained the need for an intrinsic biological dosimeter, presented evidence that lymphocyte mitochondria may satisfy that need, and described the tubidometric study of isolated mitochondria in mathematical detail. It is the intent of this chapter, applying the information from the first three chapters, to devise a dosimetry system of quantification using lymphocyte mitochondria.

In order to make practical use of mitochondrial swelling as a radiation dosimeter, it is necessary to determine a dose-versus-damage function. To accomplish this, mitochondria can be isolated, aliquots can be exposed to a range of radiation doses, and these can be subjected to osmotic swelling. The disturbance of these swelling curves by radiation can be described by a variety of damage indices. Dose-response curves can then be constructed, to select the most precise and sensitive index. It is this sort of generalized treatment which has been applied to the measurement of swelling perturbation in response to other disruptive influences.

Alternatively, the actual effects of radiation damage on the swelling process and its tubidometric

manifestation should be isolated and clearly defined. These pertubations should be measurable quantities which are predictable, reproducible, and understandable in light of the foregoing analytical development.

Once the dose-response function is established, the osmotic swelling of prior-irradiated mitochondria should deviate from the behavior of unirradiated controls in one of two ways. Isolated mitochondria should manifest anomolous swelling curves outright, or should present anomolous dose-response curves upon subsequent radiation exposure.

Quantification of Radiation Effects on Mitochondrial Swelling

If mitochondria exhibit two discrete states, one normal and the other damaged (see Figure 1), the mathematics of Target Theory may be applicable (pp. 136-144, Casarett). The two steps for the application of Target Theory to this system are: 1) the surviving fraction, S, must be determined; and 2) the number of hits per kill and the dose necessary to destroy all but 37%, D₃₇, must be determined.

Determination of the surviving fraction.

A special case of equation (3.39) for the timedependent transmittance for two groups of mitochondria is:

$$T(t) = e^{-(P_1/r_1^2 + P_2/r_2^2)}, \qquad (4.1)$$

in which the radii, r_l and r₂, and abundances, P_l and P₂, are defined for intact and damaged mitochondria, respectively.

Using the relationship between "shell thickness," a, and radius, given by equation (3.30) as follows:

$$a \alpha 1/r^2$$
; (4.2)

and substituting into equation (4.1) gives

$$T(t) = e^{-(P_1a_1 + P_2a_2)}, \qquad (4.3)$$

which can be rearranged to

$$-\ln[T(t)] = P_1 a_1 + P_2 a_2 . \qquad (4.4)$$

For the special case of a control, in which none of the mitochondria are damaged, $P_2 = \emptyset$, and at the same time, t,

$$-\ln[T(t)_{c}] = P_{T}a_{1}$$
, (4.5)

in which P_T is the total abundance of mitochondria in the sample. If P_T is arbitrarily defined as unity, equation (4.5) becomes,

$$-\ln[T(t)_{c}] = a_{1}$$
 (4.6)

Substitution of equation (4.6) into equation (4.4) yields:

$$-\ln[T(t)] = -P_1\ln[T(t)_c] + P_2a_2 , \qquad (4.7)$$

in which P_1 is now the surviving fraction of mitochondria, S. Since damaged mitochondria are assumed to be osmotically inactive, a_2 is time-independent, and if no damage occurs during the swelling process, the term P_2a_2 is constant. Equation (4.7) is more properly presented as follows:

$$\ln[T(t)] = S \ln[T(t)_{0}] - (1 - S)a_{0}; \qquad (4.8)$$

since the abundance of damaged mitochondria, P_2 plus S equals one. By the relationship between transmittance and absorbance it is possible to restate equation (4.8) as

$$A(t) = S A(t)_{c} + \frac{(1-S)}{2.303} a_{2}$$
 (4.8a)

It is possible, therefore, to use equation (4.8), or equation (4.8a), as the basis for determining both S, the surviving fraction, and a_2 , the "shell thickness" of the damaged group. This method is illustrated in Figure 4.

The slope of control curves should be one, with the intercept at zero. The slopes of damaged samples should be less than one, with intercepts that yield a consistant



value for a_2 . This value can be determined independently by the preparation of a totally damaged sample, by the same reasoning as equation (4.6),

$$a_2 = -\ln[T(t)destroyed]$$
(4.9)

This might also be a good way to test the assumption that the damaged mitochondria are osmotically inactive.

It should be noted that timing is especially critical with this method since small timing errors can result in large errors in the sample versus control ratio, especially at early times, when transmittance changes are large and especially important. This method also assumes that the basic process of swelling is either unhampered or nonexistant, which may not be the case. There may be an intermediate level of damage in which swelling proceeds, but at an anomolous rate. In order to examine this possibility, a further treatment of the swelling curves is indicated.

Transformation of swelling curves into volumetric information.

In order to more closely examine the swelling curves, it is necessary to transform the units of transmittance into arbitrary volumetric units. From equation (3.39a) for one group,

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$$T(t) = e^{-P(V^{-2/3})}$$
, (4.10)

By taking natural logarithms;

$$\ln[T(t)] = -P(V^{-2/3})$$
;

and simplifying;

$$-\ln[T(t)] = P(V^{-2/3}),$$
$$-\frac{\ln[T(t)]}{P} = V^{-2/3},$$

and inverting;

$$\frac{P}{-\ln[T(t)]} = V^{2/3}$$

and raising to the 3/2 power,

$$\frac{P^{3/2}}{-\ln[T(t)]^{3/2}} = V , \qquad (4.11)$$

we can get an equation for V, in terms of transmittance and abundance, P. This can be expressed equivalently,

$$\frac{P^{3/2}}{[A(t)]^{3/2}} = V , \qquad (4.11a)$$

in terms of absorbance units. Since the abundance, P, is not known in absolute terms (unless by microscopic sampling), the volume should be written as:

$$\frac{1}{[A(t)]^{3/2}} = \frac{V}{P^{3/2}} = Q \qquad (4.12)$$

in which the quantity, Q, is defined as the ratio between the volume, and the abundance to the 3/2 power. This ratio can be shown to be identical to the inverse of, the abundance times the shell thickness, a, or

$$Q = \frac{1}{P_a}$$
 (4.12a)

when two Q parameters are compared,

$$\frac{Q_1}{Q_2} = \frac{V_1 / P_1^{3/2}}{V_2 / P_2^{3/2}} , \qquad (4.13)$$

The ratio is given by equation (4.13).

Conversion of time dependent transmittance data into Q-data will result in numbers which, for a given sample, where $P_1 = P_2$, should be representative of relative volume changes. From this data the magnitude of swelling can be determined.

Determination of first-order rate constants.

By the empirical rate equation for swelling, equation (3.7),

$$V(t) = V_s - V_c e^{-Lt}$$
 (4.14)

Division by the totally swollen volume, V_s , yields

$$\frac{V(t)}{V_s} = 1 - \frac{V_c}{V_s} e^{-Lt}$$

which can be rearranged,

$$(1 - \frac{V(t)}{V_s}) = \frac{V_c}{V_s} e^{-Lt}$$

and reduced to the form:

$$\log \frac{V_{c}}{V_{s}} - \frac{Lt}{2.303} = \log (1 - \frac{V(t)}{V_{s}}) \quad . \tag{4.15}$$

Equation (4.15) is the equation of a line, and lends itself to the analysis as illustrated by Figure 5. Normalization of the Q-data, that is, division of each Q-value of a sample by the highest achieved Q, will result in the factor $V(t)/V_s$, for the rate constant determination. The intercept is of some use in determining the actual magnitude of swelling, and the relative numerical value of V_s .

Determination of the relative active volume.

Since the mathematical treatment of swelling and light scattering has been statistical, it is possible to describe average properties through the resultant model, using the one-group model.



Using equation (4.13), it is possible to compare the average volume of a given sample at a given time with the average volume of a control (intact) sample at the same time, provided there are the same number of particles in each sample.

$$\frac{Q(t)}{Q(t)_c} = \frac{V}{V_c} \alpha S . \qquad (4.16)$$

This relationship is valid only if the swelling process is unchanged from sample to sample, i.e., the rate constant must remain the same. If this is the case, the ratio of volume between sample and control will remain constant. This constant ratio is indicative of the fraction of intact mitochondria in the sample, and must be proportional the S, the surviving fraction.

Application of Target Theory

If mitochondrial damage is, indeed, a two state phenomenon, and if the surviving fraction, S, can be determined, it is a simple matter to analyze the results by means of Target Theory.

As illustrated by the survival curves in Figure 6, a plot of log S-versus-log dose should be constructed. The resultant curve can be interpreted to determine number of hits per kill and inactivation dose, D_{37} , defined as the dose required to inactivate all but 37%.

Another interesting bit of data which can be obtained is the effective target size. By the following relationship,

target volume(cc) =
$$\frac{1}{D_0 \times 2 \times 10^{12}}$$
, (4.17)

since D_0 is defined as the dose to produce 1 hit per target, and since 1 R will produce 2 x 10^{12} ionizations per gram (approximately per cc), the target volume can be determined. In the single hit theory, D_0 is identical to D_{37} . However, in multihit theory, D_{37} produces m hits per target, where m is the number of hits required for inactivation. Equation (4.17) must be modified, accordingly, to yield:

target volume(cc) =
$$\frac{m}{D_{37} \times 2 \times 10^{12}}$$
. (4.18)

The determination of target volume will give a means of assessment of the validity of this method. Since the sensitive target in this case is assumed to be the mitochondrial membrane, the target volume calculated should correspond with the shell volume, V_{shell}, mentioned previously, or with the volume of some discrete elements of the membrane, such as molecules of the electron transport chain, which are critical to the maintainance of gradients across the membrane.



Analysis of Swelling Curves by Numerical Methods

Since the analysis of mitochondrial swelling curves can be a monumental task, it is desirable to determine kinetic parameters and conformance of the data to different models by means of electronic computers. The analyses previously detailed in this chapter can easily be transformed into computer programs. In order to provide a more general method of analysis of swelling data, a FORTRAN program was developed. The program consists of an executive program and two subroutines (Figure 7). A complete program listing is included as Appendix C.

The executive program, EXESWL, accepts the input data, generates an initial approximation of the solution, calls the search subroutine, MNWD4A, and handles the output of the solution, once the fit is optimized.

The search subroutine, MNWD4A (MacPhate, 1976) accepts data from the executive program. MNWD4A is an extensively modified version of the algorithm of Powell (1964). This algorithm uses the method of parallel tangents to search an error surface, defined by the subroutine SWELL, and to locate an error minimum. Based on the results of this three-legged search, MNWD4A varies the values of the input parameters and searches again until the error is minimized. MNWD4A, in this configuration, has simultaneously varied as many as 40 parameters, with good results.





Subroutine SWELL defines an error surface by comparing the result of the tentative parameter values, when substituted into the swelling/transmittance model, against the observed values. SWELL also defines the contraints on the numerical value of the parameters, by adding a penalty function to the overall error of the fit, when the parameters values get out of bounds. The error in the fit is relayed to MNWD4A by the parameter COST.

As soon as the error is minimized, SWELL is called again, this time by EXESWL. The final call to SWELL returns only error in the fit, without the penalty function. EXESWELL uses this error to calculate the standard deviation, outputs the solution, and itterates the process, if multiple terms are to be considered in the model.

With the need for intrinsic biological dosimetry established, the reasoning for the choice of lymphocyte mitochondria as the sensitive organ set forth, an analytical description of the phenomena derived, and a system for quantitative dosimetry detailed, it is now the proper time to discuss the actual methods for the extraction, purification, and analysis of the organelle of interest.

CHAPTER 5

EXPERIMENTAL PROCEDURES

The procedures for the extraction, purification, irradiation, and swelling of lymphocyte mitochondria are divided into modular sections for lymphocyte isolation, mitochondrial extraction, simultaneous irradiation, and swelling. The sections are presented in chronological order. Each section consists of an overview, a protocol, and a technical comments subsection.

Isolation of Lymphocytes from Whole Blood

The purpose of the first protocol is to isolate a high yield of peripheral lymphocytes from whole blood with relatively little contamination by other cell types. The method is a modification of that by Kay and Kayberle (1972), in that the blood was heparinized as described (Demopoullos, 1963) instead of physically defibrinated. The method is rapid and inexpensive, and compares favorably with other methods of lymphocyte isolation (Willis, D., unpublished).

Protocol for lymphocyte isolation.

 Whole blood is collected in a siliconized glass or plastic flask containing 7500 USP units of heparin (ammonium salt) per liter of blood. 2) Heparinized blood is transferred to 50 ml plastic screw-top centrifuge tubes and centrifuged at 500 x G for 30 minutes, with refrigeration at 5° C.

3) The interfacial buffy coat (white cell layer) is removed by aspiration with a siliconized or plastic Pasteur pipette, without disturbing the underlying red cells. The buffy coat is transferred to plastic centrifuge tubes and is resuspended in an equal volume of Earle's Balanced Salt Solution (EBSS, Earle, 1943).

4) A large plastic syringe (35 ml) filled with cotton fibres acts as an isolation column. The syringe barrel and fibres are washed with EBSS. The washed column is then press-fitted into a 50 ml plastic centrifuge tube. Saran wrap can be wrapped around the syringe barrel to make a complete seal.

5) Approximately 20 ml of buffy coat/EBSS solution is placed on the column using a siliconized pipette. The saturated column is then allowed to incubate for 15 minutes at room temperature.

6) A suspension of lymphocytes and red cells are expressed from the column into the centrifuge tube by insertation of the syringe plunger and compression of the fibres.

7) An equal volume of Tris-buffered, 0.83% ammonium chloride, pH 7.2, is added to the lymphocyte-red cell expression and the mixture is agitated for 5 minutes.

8) Lymphocytes are collected by centrifugation
for 15 minutes at 500 X G with refrigeration
(2-5^oC) in preweighed centrifuge tubes. If the resultant
pellet is reddish in color, steps 7) and 8) are repeated.

9) Supernatant is decanted and the isolated lymphocytes are weighed, then resuspended in 0.25 M sucrose, 1 mM Ethylene Diamine (or Dinitrillo) Tetraacetic Acid (EDTA), Tris buffered at pH 7.2. This suspension buffer is referred to as MSB (mitochondrial suspension buffer) throughout the remainder of this chapter.

<u>Technical comments on lymphocyte isolation</u>. The concentration of heparin is important for a good isolation (Campbell, 1964) because an excess will cause coagulation of the lymphocytes, which sometimes traps other types of blood cells. Either silicon-coated or plastic glassware are used to maximize the yield of lymphocytes, which tend to stick to bare glass. The suspension medium, EBSS, is not calcium and magnesium free in order to preserve mitochondrial function, which depends on these divalent metal ions. Cotton fibers are obtained from sterile cotton gauze or cheesecloth. The isolation procedure can be expedited by the use of several columns. Methyl green-

pyronin stain can be used to check purity of the lymphocyte preparation (Kay and Kayberle, 1972; Clark, 1973).

Extraction of Mitochondria from Lymphocytes

The extraction of mitochondria from lymphocytes was achieved by homogenization and differential centrifugation in isoosmotic sucrose. Detailed discussion of this method and alternative approaches are set forth in Appendix B.

Protocol for extraction of mitochondria.

Suspended lymphocytes are collected at
 Suspended lymphocytes are collected at
 G with refrigeration for 15 minutes. After
 discarding the supernatant, lymphocytes are resuspended
 in fresh MSB.

2) Lymphocytes are homegenized to rupture the cell membrane by means of a hand operated Dounce homogenizer. Homogenization is conducted in an ice bath for 15 minutes or until no intact lymphocytes are visible under light microscope. Homogenate is transferred to glass centrifuge tubes with plastic inserts.

3) Homogenate is centrifuged at 500 X G for 10 minutes with refrigeration, to collect nuclei and cell debris. Mitochondria remain in suspension. This step can be repeated.

4) Suspended motochondria and microsomes are pipetted off into glass centrifuge tubes. Cell debris pellet can be resuspended and recentrifuged to improve yield. Suspended motochondria are collected at 4000 X G for 10 minutes refrigerated. Microsomes remain in suspension.

5) After discarding the supernatant, the mitochondrial pellet is resuspended in MSB and pelleted by centrifugation at 8700 X G for 10 minutes with refrigeration. Steps 3) and 4) can be repeated for increased purity.

6) After discarding the supernatant, mitochondria are resuspended in minimal volume of MSB and are refrigerated.

7) Protein concentration is determined by means of a modified Biuret assay, which assumes an extinction coefficient of 0.095 for 1 mg/3 ml volume of Biuret complex.

8) Mitochondria are diluted to 0.75 mg/ml extractant protein concentration and 1 mg/ml Bovine Serum Albumin (BSA), using 4 mg/ml BSA in MSB and MSB as diluents.

Technical comments on mitochondrial extraction.

Homogenization of lymphocytes is especially easy because of their adhesion to the glass walls of the homogenizer. Additional washing is performed if the pellet appeared visually impure. Because of the low temperature of the sample, incubation with Biuret reagent was allowed to proceed at room temperature for a full 60 minutes before observation with the spectrophotometer at 540 nm. Since the incubation time is so long, the protein assay is run in duplicate to avoid unnecessary delays. The addition of BSA to the mitochondrial fraction is a wellknown measure designed to prevent the degenerative tendancy of the organelle outside the cell (Spenser and Horton, 1978). The low temperatures maintained during centrifugation should be sufficient to avoid damage to the membranes from hydrostatic pressure (Wattiaux-deConinck, <u>et al.</u>, 1977).

There is one final consideration which has bearing on the method of extraction of lymphocyte mitochondria to be used as intrinsic biological dosimeters. There may be an increase in the fragility of the organelle associated with radiation damage. Since the homogenitation procedure used here is rather rough on the organelles, only intact mitochondria tend to be isolated, causing interpretational difficulties (Locher, <u>et al</u>., 1978). This problem has been surmounted by the method of Jennings, <u>et al</u>. (1969), which uses an enzyme Nagarse. This method has demonstrated the ability to isolate damaged as well as intact mitochondria. This method should be used when isolating lymphocyte mitochondria for dosimetry.

Irradiation of Isolates and Dosimetry

In order to provide simultaneous irradiation at a large range of exposures, the ⁶⁰Co irradiation facility at LSU Nuclear Science Center was used. The irradiation configuration is illustrated in Figure 8.



Figure 8. Co⁶⁰ Irradiator Facility

Sample containers (bunnies) were attached to a weighted rope at premeasured positions. Single CaF2:Mn Thermoluminescent Dosimeters (TLD), cleared of residual excited electrons by overnight heating at 400°C, were heat-sealed inside short pieces of plastic tubing and placed inside each bunny. Individual screw-top 1/2 dram glass bottles, to hold about 1.5 ml of sample each, were filled with water for a field check and were placed inside each bunny. The entire apparatus was quickly introduced into the water-filled irradiation tank by means of a preplaced polyvinyl chloride (PVC) pipe, open at both ends, which acts as a guide to provide relatively reproducible geometry. When emplacing the PVC pipe, care was taken to allow water to fill the pipe to avoid compromising the biological shield. After irradiation for a timed interval the rope assembly was raised, placed on an ice bath, and transferred to a spectrophotometer. The TLD's were read at 24 hours post-irradiation to constitute a record of relative exposure absorbed by each individual sample.

Induction and Observation of Swelling

The purpose of this procedure is to subject the mitochondria to a set of conditions which will cause a reproducible response as evidence of the mitochondria's degree of integrity. The strip chart preserves a record of this response for later reduction and analysis.

Protocol for swelling.

A double beam spectrophotometer is zeroed at 1) 546 nm using 3 ml cuvettes each containing the reaction mixture (0.5 ml BSA at 6 mg/ml; 0.5 ml potassium phosphate monobasic, KH_2PO_4 , 0.24 M; 0.5 ml KCl, 1.2 M; and 0.5 ml Tris, 0.12 M pH 7.2) plus 1 ml BSA at 1 mg/ml in MSB to act as the sham sample.

The sample cuvette is cleaned and replaced in 2) the spectrophotometer. The 1.5 ml mitochondrial sample is added to the cuvette and the initial absorbance is recorded.

The sample is removed from the cuvette; the 3) cuvette is cleaned; and 2 ml of reaction mixture are added to the cuvette.

4) One ml of the mitochondrial sample is added to the cuvette; the strip chart is turned on as a record of the start time; and the cuvette can be covered and inverted several times for mixing. The cuvette is returned to the sample chamber which, when closed begins recording of data.

5) After 10 minutes the test is terminated. sample is recoverable in its present state. The entire process is repeated for the suceeding samples.

Technical comments of swelling. The procedure for mitochondrial swelling comes from Hunter and Smith (1967). See also Packer, 1967. It is called "pseudoenergized" swelling because of the attempts to correlate it to energy

The

function in mitochondria. Nevertheless, by the judicious choice of reaction conditions the method manages to produce 3-4 times the magnitude of simple osmotic swelling (Jung, <u>et al.</u>, 1977). This is because of the rapid transport of ions in the reaction medium into the mitochondrion, which in turn causes increased water uptake.

The reaction mixture and sample are rather viscous, so that mixing may be a problem. Experience has shown that this mixing problem is observable in 1 ml cuvettes, but not in 3 ml cuvettes.

The viscosity of the solution can be significantly reduced by the use of mannitol instead of sucrose (50% lower viscosity) in the MSB, or by the reduction of BSA or deletion of BSA altogether.

Reproducible mixing and more accurate initiation timing can be provided by a crude sample injection system based on the "stopped-flow" concept.

CHAPTER 6

EXPERIMENTAL RESULTS AND DISCUSSION

Using the experimental methods outlined in Chapter 5, peripheral lymphocytes and mitochondria were obtained, irradiated and subjected to conditions to cause swelling. The resultant swelling data were reduced as described in Chapter 4. The presentation of these results is in chronological order.

Discussion of Experimental Procedures

Whole blood was obtained from aortic puncture of a single, freshly-killed cow at a local slaughter house. Because of the brief duration of the experiment, no antibiotics were added to the suspension media. The red cell expansion was repeated to minimize the number of remaining erythrocytes, and was followed by a wash in MSB. This wash was to remove as much hemoglobin on mitochondria (Pettengill, 1974). The purity of the lymphocyte preparation was checked microscopically after staining with Janus Green B (Brenner, 1949). The yield of lymphocytes was approximately 10 gram wet weight/liter whole blood.

The degree of homogenization of the lymphocytes was checked with and without staining by Janus Green B (Clark, 1973) by phase contrast microscopy. Protein was determined by the method of Gornal, <u>et al</u>. (1949), using

TABLE 1

Dosimetry Results

		1	Dose (rad) in			
Distance (cm) from bottom		Field Checks 2 (5 min)	2 (2 min)	Range Finding	Experiment (estimated) Fr	nent From Fig. 3
50		1		(1000)		
60 70		1.970 .980	788 392		(001)	(275)
75 80		.586	234.4	(001)	(78)	(200)
85 90	36.4	.254	101.6			(105)
95		.151	60.4			(22)
105	9.7	.63	25.2	(10)		(28)
1150		33.4	13.36		(2) (2)	(15)
125	3.19	19.7	7.88		(3)	
130 150	1.05	6.8 5.32	2.72 2.128	(1)	(2) (1)	(4) (2)
160 170	.49	<u> </u>	+ F			
190	.25	. 40 	.16			6
210 210 220	.035	.12	.048	(.1)		2

Y		3)		5. 5.	
		rom Fig.			63
		ure Experiment (estimated) (f		stimated estimated (TLD reader broken)	
	(p	in 2 min exposure Range Finding (e		estimated (TLD read	
	TABLE 1 (cont'd)	Dose (rad) : 2 (2 min)		Calibrated from #2	
	E	Field Checks 2 (5 min)	.00 .00 .38 .338 .338 .337 .338 .377	.27 recalibrated after 240 cm	
			.0164 .0171 .0107 .0098 .0176 .0125 .0112 .0125 .0125 .0130	. 25	
		Distance (cm) from bottom	230 240 250 250 250 250 250 250 250 250 250 25	Empty pan Remarks:	


Figure 9. Radiation Field Check





BSA as a standard. The yield of mitochondrial protein was approximately 30 μ g/ml whole blood, or 0.3% of the lymphocyte wet weight. Since a 0.75 mg sample is used in the swelling assay, 25 ml whole blood is required per sample. The total reaction volume is 3 ml, so the possibility of a microadaptation is not unrealistic.

A field check with water phantoms was conducted as previously described. The results of the field check are presented in Table 1 and Figure 9. The half-thickness calculated for water and radiation of 1.25 MeV (average energy per disintegration for 60 Co), from Figure 9 is 11 cm which is in good agreement with accepted values.

In order to provide a bracketting of irradiated samples, the first sample which was swollen was a control. This sample was followed by the most highly irradiated sample and the other samples in decreasing order of exposure. The last sample which was read was also an unirradiated control. The order of assessment was twofold: If there was significant degeneration over the waiting time for swelling, this would be demonstrated to its fullest extent in the controls, and any time damage effect would tend to mask radiation damage rather than to amplify its effect. While one sample was swelling, the other samples were kept on ice. The spectrophotometer was was chamber at ambient temperature. Samples were not morphologically characterized post irradiation.

A range-finding study of five samples indicated that the swelling curves exhibited abnormalities around the 10 rad dose. Positions were chosen to bracket this area.

Swelling curves were manually digitized with a 0.5 minute step size. The tabulated data is presented in Table 2. It is obvious from these data that there is a decreasing trend of transmittance with increasing dose.

The data were subsequently transformed into Q-data, by the use of equation (4.12). These data are reported in Table 3. From this data it is evident that the magnitude of the volume changes is relatively constant, about 1.52 X start volume.

In order to determine the first order rate constants, the data were further reduced by normalization, as described previously. Data suitable for use in equation (4.15) is presented in Table 4. The rate constants were determined by a linear-least-squares variation of Figure 5. Graphs of the form of Figure 5 were prepared for visual inspection. These graphs are included as Figures 11-16. The values of the rate constants do not vary significantly from the average value of 0.406 + 12% min^{-1} . Variations between samples and nonlinearity of the graphs can best be understood by reference to the well-known dependence of the rate constant on temperature,

TABLE 2. Digitized Swelling Data

S6 20	43 45 49 49 50 51 51 51 51 53 51 53 53 53 53 53 53 53 53 53 53 53 53 53
S5 15	43 43 45.5 49.5 50.9 50.9 51.1 51.2 51.2 51.2 51.3 51.3 51.9 51.3 51.9 51.9
S4 11 VCE	47 48.5 51 52 533.4 554.5 54.5 54.5 54.5 54.5 54.5 54
S3 8 TRANSMITTANCE	45 47 49.5 50.8 51.2 51.2 51.2 51.2 51.2 51.2 52 52 52 52 52 52 52 52 52 52 52 52 52
S2 4 PERCENT TR	49 51 55 55 55 55 55 55 55 55 55 55 55 55
s1 2 PI	53 55 57 57 57 57 57 57 57 57 57 57 57 57
c2 0	57 58 59 59 59 59 59 50 60 50 61 61 61 61 61 61 61 61 61 62 62 52 36 52 36 52 36 52 36 52 36 52 36 52 36 52 36 50 53 59 55 59 55 59 59 50 50 50 50 50 50 50 50 50 50 50 50 50
C1 0	55 60 64 64 65 65 65 65 65 65 65 65 65 65 65 65 65
Sample Dose (rad)	

TABLE 2. (continued)

12 15.3 19.8 19.8 19.8 223.5 223.5 223.5 223.5 223.5 223.5 223.5 224.0 224.0 S14 275 v.u.80.0001.08 ∞ 30077 S13 200 S11 S12 100 140 TRANSMITTANCE 08101010101010 010 υœ S10 75 PERCENT 55 N N S84040 .5 .3 4.00 9.480 01400H . . • • 555555566 S7 28 Sample Dose (rad) Time (rad) *NONONONONONONONONON*

TABLE 3. "Q" Values

S6 20	N0UN80H2W4N00V880000 H	9C.1
S5 15	00000000000000000000000000000000000000	L.4/
S4 11	+++++mm75H000870m00m	L.4U
S3 8 UES	000000000000000000000000000000000000000	L.30
S2 4 Q VAL		L.44
S1 2	00000000000000000000000000000000000000	L.42
C2 0	77000000000000000000000000000000000000	1.29
C1 0	7.56 9.57 11.12 11.12 11.72 11.72 11.72 12.63 12.63 12.63 12.63 12.63 12.63 12.63 12.79 12.63 12.79 13.12 13.12 13.12	1.75
Sample Dose (rad) Time (rad)	11 0.0000000000000000000000000000000000	Qs/Qo

TABLE 3. (continued)

82 45 S1 27 . • • -02 S13 200 **tttttt** \sim ഗ S12 140 \mathfrak{C} 63 S11 100 -VALUES 338162558667707661542333 3381625586677066154233 338162558667707 60 S10 75 . . . -0 70 59 . tbtbtbtbtbtbtbmmmmnn 1 777730866308874388688 51 . . . ٠ \circ S8 40 _ 24443339516914063200320 54443322209914003200320 58 S7 28 _ Sample Sse (rad) ime (rad) nononononononononon 000008844000066 Q_s/Q_o Dose Time

TABLE 4. Normalized Volumetric Data

.359.242.242.175.175.175.175.175.175.175.033.038.038.038.0330.021.017.001S6 20 S5 15 5 I 1 I S4 11 $\infty \omega$ Q/Q_s S 1 .304 .241 .241 .171 .171 .171 .092 .0080 .0072 .0072 .0072 .0072 .0072 .0072 .0072 .0073 .0073 .0075 S2 (1 S1 2 00051 C2 0 $\begin{array}{c}
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(430)$ 010 (rad) (rad) Sample 09988776655449332221100 Dose Time

TABLE 4. (continued)

Re	Results of	of Linear Least-Square Fit for Preceding Data	ist-Square	Fit fo	r Prece	ding Dat	0	
	- I		r.			C		
Correlation	.972	799.	.984	. 984	.993	.949	.986	.981
Intercept (V_{c}/V_{s})	.399	.307	.344	.447	444	.295	.335	.522
Slope k(min ⁻¹)	.360	.429	.357	.439	.768	.402	.368	907.
Note: Avera	Average k is	.430 ± 24%.	Discard	ing 53	results	in an a	Discarding 53 results in an average k of	of

.406 + 12%.

TABLE 4. (continued)

Sample Dose (rad) Time (rad)	57 28	S8 40	55 55	s10 75 (1 - Q/	S11 100 (_Q)	S12 140	S13 200	S14 275
0442288444666666888990 202020202020202020202020202020202020			.412 .334 .334 .158 .158 .098 .0087 .0087 .0087 .0087 .0087 .0087 .0087 .0087 .0087 .0087 .0053	. 087 . 047 . 005 	. 387 . 387 . 232 . 191 . 149 . 128 . 091 . 091 . 002 . 028 . 028 . 028 . 028 . 028 . 021 . 007 . 011	. 197 . 164 . 197 . 128 . 099 . 0083 . 012 . 008	0009	$ \begin{array}{c} 451\\ 272\\ 272\\ 272\\ 272\\ 175\\ 087\\ 053\\ 063\\ 063\\ 029\\ 010\\ 010\\ 010\\ 010\\ 010\\ 010\\ 010\\ 01$
1								

TABLE 4. (continued)

								190
	Results of	s of Linear Least-Square Fit for Preceding Data	st-Square	Fit fo	or Prece	ding Dat	ta	
Correlation	n .993	.986	.991		066.	. 995	.983	.981
Intercept (V_{c}/V_{s})	.398	. 464	.555	8	.480	.352	.590	.521
Slope k(min ⁻¹)	.351	.490	.417	l ł	.423	.497	.354	.390
Note: Ave	Average k is	is .430 + 24%.		ing 53	results	in an	Discarding 53 results in an average k of	of

C • | .406 ± 12%.



Figure 11. Swelling Rate Constant Determinations for Samples Cl and C2.



Figure 12. Swelling Rate Constant Determination for Samples S1-S3.



Figure 13. Swelling Rate Constant Determinations for Samples S4-S6.



Figure 14. Swelling Rate Constant Determinations for Samples S7-S9.



Figure 15. Swelling Rate Constant Determinations for Samples S10-S12.



Figure 16. Swelling Rate Constant Determinations for Samples S13 and S14.

as illustrated by the Arrhenius equation (Daniels and Alberty, 1966) which is

$$-E_{a}/RT$$

$$k = Ae$$
(6.1)

The agreement of the rate constants indicates that the permeability to water of those mitochondria active in swelling is unaffected by any damage they may have received from the radiation.

An attempt to determine the surviving fraction directly from the relation given by equation (4.8) and Figure 4 was unsuccessful, as shown in Figure 17. The slope of these curves, as revealed by statistical analysis (see Table 5), increases with radiation dose, rather than the expected trend. Figure 18 depicts the dose dependence of the reciprocal of the slope, which bears an uncanny resemblance to the typical survival curve in Figure 6. The inset of Figure 18 hints at a possible cause for the failure of the direct method. The parameter a2 from equation 4.7 is not constant, as assumed. Either damage occurs during swelling or the transition from the osmotically active state to inactive is not a simple, discrete phenomenon, and intermediate swelling of damaged mitochondria may occur.

Using equation (4.16) and the average Q values of the controls, the data were again transformed. This TABLE 5. Data for the Direct Determination of

S

S6 20 S5 15 S4 11 S 33 -S2 4 -ln[T(t)] . . S1 2 C2 0 0 C1 (rad) (rad) Sample Dose Time

TABLE 5. (continued)

Linear Least Square Fit of ln T(t) versus ln T(C $_2$) For Preceding Data	e Fit of ln	T(t) vers	us ln T(C ₂)	For Pre	eceding Data	
Correlation	.994	.997	.987	.994	066.	. 998
Intercept (V _c /V _s)	139	213	180	186	256	477
Slope k(min ⁻¹)	1.36	1.63	1.716	1.662	1.918	2.336
Intercept divided by slope	102	126	105	112	134	204

TABLE 5. (continued)

TABLE 5. (continued)

B		. 702	-1.822		6.825		3267		
ding Dat		.982	1 393		4.673		298		
for Prece		.995	705	104	1 83/	t-0.T	057		
	4	.987		659		2.9/8	110	477	
T(+)] versus		995		935		3.752		249	
	Fit or unl	000	066.	382		2.305		166	
	: Square I		166.	251		1 701	•	148	
	Linear Least Square		_					divided	
	Lin		Correlation	Intercept	(^v c ^v s ^v	Slope_1	k(min ⁻)	Intercept divided hv slope	







Figure 18. Dose Response of Parameters from Table 5.

transformation is a means of expressing the fraction of active mitochondria, or another expression for S. The S values thus determined are reported in Table 6. Notice that the value obtained shows little variation within a given sample but large variation with increasing dose. Also note the small variation between the control values. These observations are consistent with the arguments detailed in Chapter 4 that this value is indeed the surviving fraction, S.

The values given for S can therefore be plotted by the method of Figure 6 and evaluated with respect to target theory. This plot is reproduced as Figure 19. The scatter of data on this plot is significant enough to prevent definitive analysis by Target Theory, but a rough approximation is possible. The shape of the curve appears to exhibit a knee at about 100 rads. This shape is consistent with the multiple hit/multiple site model.

Extrapolation of the 'linear' region past the knee yields an intercept of about 0.73 which corresponds to a value of 5.4 hits (sites) per kill.

The dose necessary to kill all but 37% of the mitochondria can be read from the graph directly. Because of the scatter in this region, there is some uncertainty in the value. The value is apparently between 100 and 165 rads, regardless of the assumed shape of the curve.

TABLE 6. Q/Q_C Values (S)

568 S6 20 . 552 S5 15 629 S4 11 571 833 8 694 \$2 4 Q/Q_{c} 820 S1 2 920 02 2 10 CJ 60 . --1 e _____ ~~~~ -4 -1 -00 Sample Dse (rad) ime (rad) S vovovovovovovovovovovovoAverag Dose Time

TABLE 6. (continued)

		Linear Least S	Linear Least Squares for Preceding Data	Data		
Analysis of Q/Q_C Values	Mean	Standard Dev.	Fit of Q/Q _e Data	Correlation Slope Intercept	Slope	Intercept
all points incl.	.586	.586 ≠.286 (38.9%)	all points included	.857	223	.859
w/out Cl	.553	553 ≠.191 (34.5%)	w/out S10	.892	235	.865
w/out C1, S14	.580	≠ .163 (28.2%)	w/out S10, S7	.935	234	.850
w/out C1, C2, S14		.554 ≠.136 (24.6%)	(24.6%) w/out S10, S7 & S4	.933	232	. 844

TABLE 6. (continued)

ŧ		1
S14 275		5
S13 200		
S12 140	441 4441 4441 4441 4441 4441 4441 4442 4441 4442 4441 4442 4441441	4 - -
S11 100	410 410 410 410 4422 4442 4442 4442 4442	٦ C
s10 75 Q/Q _c	741 .741 .633 .633 .6629 .6629 .6629 .6629 .5888 .5888 .5755 .5759 .57559 .55559 .555	D D
s9 55		>
58 40	483 483 483 483 488 474 476 474 476 478 4778 4778 4778	t c
57 28	730 694 696 696 699 699 693 693 693 693 709 709 709 709 709 709 709 709 709 709	CC0.
Sample Dose (rad) Time (rad)		Average o

93 Intercept .865 .850 .859 . 844 Correlation Slope -.223 -.235 -.234 -.232 .933 .857 .892 .935 Linear Least Squares for Preceding Data all points included ≠.136 (24.6%) w/out S10, S7 & S4 TABLE 6. (continued) Standard Dev. Fit of Q/Q_e Data w/out S10, S7 ≠.191 (34.5%) w/out S10 *≠*.163 (28.2%) ≠.286 (38.9%) .553 .554 .580 Mean .586 w/out C1, C2, S14 all points incl. w/out Cl, Sl4 Analysis of Q/Q_C Values w/out Cl





By equation (4.18), the using the values reported above, the target size is calculated to be between 1.6 x 10^{-14} and 2.7 x 10^{-14} cc. Using the assumptions of the mathematical treatment of Chapter 3, the volume of the spherical shell formed by the membranes is 5.5 x 10^{-14} cc, with the average dimensions reported by Racker (1970).

The data from Table 6 were analyzed by Probit Transformation (Litcchfield and Wilcoxon, 1949), depicted in Figure 20. The percentages of damaged mitochondria (unity minus the surviving fraction, times 100%), were taken to represent the area under a Normal Distribution function between negative infinity and a point, c. The probit values, which can be obtained from a table or read directly from a special type of graph paper, are numerically equivalent to the Normal Deviation at the point, c, times 100. Analysis by this method yields a D₃₇ value of 171 rads, and an LD₅₀ value of 46 rads.

The swelling data was further analyzed by means of the computer program described previously. The data generated by the computer-derived solution agrees favorably with the actual observed data, as illustrated by Figure 19. The deviations in the shape of the observed curve from that predicted by the computer solution may be a result of temperature variation, transport phenomena (see Figure 3), or nonideal variation in shape with swelling.

The results of the single term model computer runs are summarized in Table 7. There appears to be no pattern to the variation in the computer program's ability to fit the data with the prescribed model, as evidenced by the similarities in the standard deviations. Increasing the number of terms to a maximum of ten had little effect in the overall fit of the model.

The rate constants determined are similar in value and uniformity to those obtained by the graphical method. The parameter for the overall change in volume also shows little variation, especially when normalized by division by the parameter for the totally swollen volume.

The final volume is the parameter which reflects the effect of increased radiation dose. When the final volume parameter for a sample is divided by the final volume for the control, the result is very similar numerically to the Q/Q_c value, which was used as the survival fraction, S. A plot of the values versus dose, presented in Figure 22, yields a D_{37} of 178 rads, and approximately 4 hits per kill. The target sizes, 2.8 x 10^{-15} cc and 1.1 x 10^{-14} cc, for the single hit and multiple hit models respectively, are in close agreement with values determined by the other methods.

It is of some interest to examine the results of the two term model, since the rationale for radiation damage involves the transition to a condensed, osmotically

TABLE 7. Summary of Computer Results

Sample Dose (rads) Parameter	C1 0	C2 0	S1 2 BEST	S1 S2 2 4 BEST-FIT VA	S3 8 VALUE	S4 11	S5 15	S6 20
P (abundance)	766.	.998	.998	.998	.998	766.	266.	.998
S (swollen size)	3.67	3.08	2.78	2.38	1.89	2.13	1.87	2.02
C (volume change)	.208	.860	.962	.860	.683	.758	.727	.856
K (rate constant)	.702	.371	.402	.367	.612	409.	.472	.330
Standard Deviation	.457	.051	.158	.130	.097	.098	.140	.132
C/S	.057	.279	.346	.361	.361	.356	.389	.424
S/S controls (survival fraction)	1.08	.913	.824	.705	.560	.631	.554	.599

TABLE 7. (continued)

Sample Doce (rads)	S7 28	58 40	5 5 8	S10 75 BEST-FIT	S11 100 VALUE	S12 140	S13 200	275
Parameter								
d	.998	766.	766.	766.	766.	.998	998	. 997
(abundance) S	2.44	1.64	1.28	1.87	1.50	1.47	1.32	.581
(swollen size) C	906	.684	.634	.432	.715	.481	.774	. 315
(volume change) K	337	.470	.386	1.29	.450	.454	.402	.452
(rate constant)				207	.176	.072	.443	.247
Standard Deviation	.139	.128 .417	. 495	.231	.447	.327	.586	.542
C/S S/S controls	562		.379	.554	444.	.436	.391	.172
(survival fraction)							ĕ	


Figure 21. A Typical Swelling Curve Sample C-2



inactive state. The program approaches the problem of multiple groups by starting with a number of identical groups and attempting to improve the fit by unequal modification of the terms. The results of the two term model were either to find no fit better than the two identical group case, or to force one group to assume a "dummy" role, that is, to swell very slowly, or not at all, or to swell a large amount very rapidly in order to avoid participation of that group in the calculations. This inconclusive result can probably be remedied by demanding more significant figures for convergence. Nevertheless, the result is supportive of the idea of a background of relatively inactive material which does not participate in swelling.

One anomolous swelling curve was observed. That sample, S-10, was delayed after the initiation of swelling, so that the reaction was followed to a later than normal time. An interesting similarity was noted between the sample curve and the time course of a leaky osmometer described by Katchalsky and Curran (1967). Their illustration is reproduced here as Figure 23. The sample received about D_{37} rads; this is in the region where the mitochondria have each received, on the average a destructive dose.



There is a very basic limitation on the use of mitochondrial damage as an indication of radiation damage. Mitochondrial damage can be caused by a variety of things from the isolation method to pathological conditions of the subject. The use of mitochondrial dosimetry will probably be limited to the screening of suspected exposure subjects. There may also be a time limit on the damage information carried by the mitochondria <u>in vivo</u> because of membrane repair mechanisms. These subjects are beyond the scope of this thesis.

CHAPTER 7 SUMMARY AND CONCLUSIONS

The introduction of this thesis critically examined the conventional methodology for the evaluation of personnel radiation dose. The contention was made that lymphocyte mitochondria might be suitable as a limiting indicator of radiation dose. The reasoning behind the selection of lymphocyte mitochondria as the candidate for an intrinsic biological dosimeter was explored in some detail in the second chapter. It was suggested that radiation might have some effect on the osmotic properties of the mitochondria, as evidenced by some change in their swelling response. Emphasis was placed on the significance of this damage, since energy production by the mitochondrion is dependent on the integrity of the inner mitochondrial membrane.

In order to detect changes in mitochondrial swelling, a detailed mathematical analysis of the process, and its manifestation by nephelometry, was presented in Chapter 3. The results of this treatment include an important restatement of classical scattering theory, which is derived in a simple manner, without the inappropriate assumptions of the conventional method, yet which bears

striking resemblence to the classical result. A method for the application of the theoretical treatment of swelling to the quantitation of radiation dose was described in Chapter 4. The means to analyze the mitochondrial "survival" curves by conventional Target Theory is also revealed.

Experimental methods for the isolation and analysis of lymphocyte mitochondria were outlined in Chapter 5, including the method of irradiation and dosimetry. The results of actual experiments involving the irradiation of isolated mitochondria were reported and discussed in Chapter 6. The data do not allow an unambiguous choice between single hit and multiple hit mechanisms. Analysis by either method, however, reveals a target size on the order of magnitude of the volume occupied by the mitochondrial membranes.

The theoretical upper and lower limits of detection by this method of dosimetry can be inferred from Figure 19. The variation between survival fractions determined for nonirradiated controls was 0.070. The lowest credible difference that could be measured between samples is about twice this value or 0.14. A difference of 0.14 from the control value of 1.00 gives a survival fraction of 0.86, which corresponds to a radiation dose of 2.25 rad on the survival curve. This is, therefore,

the theoretical lower limit of detection. The upper limit of detection would be the dose at which the surviving fraction could not be reliably distinguished from zero, or S = 0.14. This fraction corresponds to a dose of over 1000 rads if the single hit mechanism is correct, or 250 rads, if the damage is by multiple hits.

In addition, the following conclusions can be made:

Peripheral lymphocyte mitochondria can be obtained in quantity and quality suitable for dosimetric purposes.

Osmotic swelling traced by nephelometry, can reveal information about radiation damage to these mitochondrial isolates.

The first-order rate constant for the swelling process can be derived from the reaction time course, but derivation in the linearity of these determinations implies that the process is not strictly first-order.

Attempts to calculate the surviving fraction, S, directly demonstrate that the two-state model is not an entirely adequate description of the radiation damage phenomenon.

The osmotically active volume, Q/Q_c , provides useful information about the surviving fraction. The numerical method of analysis of the data, by the FORTRAN program is capable of providing the same information about rate constants and degree of damage.

It is clear that a degree of radiation damage to isolated mitochondria can be quantitated through the analytical methodology presented in this thesis. The observation of the loss of osmotic activity at low doses of radiation, viewed in light of the mechanistic discussion of the action of uncouplers of oxidative phosphorylation (Chapter 2), implies that radiation acts to violate the structural integrity of the mitochondrial membranes. In this respect, peripheral lymphocyte mitochondria may indeed fulfill the need for an intrinsic biological dosimeter. However, there are several critical uncertainties about the use of these organelles for personnel dosimetry.

Is it possible to isolate mitochondria from peripheral lymphocytes without perturbing the existant proportions of damaged and functional mitochondria? The enzymatic isolation procedure of Jennings <u>et al</u>. (1969) should be used to isolate mitochondria from lymphocytes which have been irradiated <u>in vivo</u> or in the form of whole blood, using good dosimetry, and the analytical methodology applied to these organelles. If the survival curves are similar to those of the irradiated isolates, further investigations are in order.

At what rate does the organism repair or replace the damaged mitochondria? The biological half-life for mitochondrial constituents is about 20 days, which places an upper limit to the usefulness of this method, but repair could be affected more rapidly. Whole animal irradiations with delayed sampling would answer this question.

What modifications of this methodology can provide increased reliability for the measurement of mitochondrial damage? Experiments should be done using temperaturecontrolled conditions during swelling, with reproducible mixing using pseudo-stopped-flow sample injection. Following swelling, samples should be morphologically characterized with phase-contrast, or, better still, electron microscopy. The measurement of oxidative phosphorylating ability would provide another measure of mitochondrial functional integrity.

Is there another method of analysis of the functional integrity of the mitochondrial population which may supplant the swelling analytical method for quantitation of mitochondrial damage? Organelle electrophoresis (mentioned in Appendix B) may provide a simpler method for the study of the mitochondrial survival. Experiments to determine the effect of radiation on the

migration pattern of mitochondrial suspensions should be conducted. It is expected that effects similar to those of uncouplers will be observed. This method has the advantage of physically separating mitochondrial subpopulations for further study.

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APPENDICES

APPENDIX A

A SURVEY OF CURRENT STRATEGIES FOR QUANTITATIVE ISOLATION OF PERIPHERAL BLOOD LYMPHOCYTES

Diana G. Willis

Most lymphocyte isolation procedures begin with preliminary processing of whole blood. Whole blood is collected in siliconized glassware or plastic containers, otherwise the lymphocytes will adhere to the glass and be lost (Wildy and Ridley, 1958). Anticoagulants such as heparin or citrate are used, or the blood is defibrinated either by passage through an ion exchange column (Greenwalt, 1962), or the use of wooden applicator sticks (Kay and Kayberle, 1972). Low speed centrifugation of the blood now produces three characteristic phases. At bottom, the erythrocyte layer comprises about 46% of the total blood volume. On top of the red cell pack a thin, buff colored layer, called the "buffy coat," forms, comprising 19% of the total volume and containing the lymphocytes, granulocytes, and leucocytes. The supernatant resulting from such a low speed centrifugation is known as the serum. Collection of the buffy coat is then accomplished by simple aspiration or by the "floatation method" (Burrin et al., 1965). Much of this fraction is made up of contaminating platelets, granulocytes, and erythrocytes which must be removed by further processing.

Perhaps the most widely used method of separating the lymphocytes from the other buffy coat material is by isopycnic density gradient centrifugation. This involves layering the buffy coat on a preformed gradient containing erythrocyte clumping agents, such as Ficoll/Hypaque (Boyum, 1968) or Sodium Metrizoate-Ficoll (Laissue <u>et al.</u>, 1975), and then centrifuging at high rotor speed to equilibrium. At equilibrium, the lymphocytes form a band at the point in the gradient which matches their own density, and any contaminating erythrocytes from a pellet at the bottom of the tube. The lymphocytes are then collected by aspiration or drainage of the tube and are resuspended in the appropriate balanced salt solution for analysis.

The fiber method applies the difference in adsorption of lymphocytes and granulocytes to nylon (Greenwalt, 1962) or cotton fibers (Kay and Kaeberle, 1972) in order to exclude granulocytes from the suspension. Unlike the glass bead (Garvin, 1961) and glass wool columns (Johnson and Garvin, 1959) from which the lymphocytes had to be eluted with a chelating agent, the lymphocytes can pass freely through the fiber columns while the granulocytes and platelets are retained. Removal of erythrocytes may be accomplished by a variety of hemolysis techniques (Fallon <u>et al</u>., 1962; and Marks <u>et al</u>., 1962). The cotton fiber technique has been combined with the Ficoll-Hypaque procedure with good results (Kay <u>et al</u>., 1976).

Once isolated, the lymphocytes must be characterized with respect to their homogeneity and functional integrity. Purity of the suspensions can be determined histologically (Clark, 1973) using Wright-stained smears or by observation of live cells using phase contrast microscopy (Rabinowitz, 1964). The functional state of the extracted lymphocytes can be established by observation of their ameboid mobility; their phagocytic ability, as evidenced by the engulfing of polystyrene beads; trypan blue staining, in which nonviable cells become stained; and by the presence or absence of the ability to conduct oxidative metabolism, as indicated by oxygen consumption observed on the Warburg manometer or oxygen polarimeter.

Methods which require isopycnic focusing call for extended periods of high speed centrifugation, typically 12 hours or more. These also require ready access to sophisticated ultracentrifugation equipment. Laissue et al. (1976) report yields of greater than 75% leucocytes with less than 1% erythrocytes and platelets present, and no contaminating granulocytes following isopycnic focusing in a liquid silicon solution. Trypan blue positive cells were rarely observed. Similarly, Yakir et al. (1977) were able to isolate 1 to 2 x 10^6 lymphocytes/ml of peripheral blood in suspensions containing 80 to 90% lymphocytes using the Ficoll-Hypaque gradient. Suspensions with greater purity can be produced in shorter times with

relatively crude equipment by fiber column methods. Concentrated suspensions of 0.5 to 3 x 10^6 lymphocytes/ml can be produced by passage through a nylon fiber column (Greenwalt <u>et al.</u>, 1962). These isolates can be stored satisfactorily for 14 to 21 days. Yields of 10^6 lymphocytes/ml whole can be obtained with less than 1% contaminating granulocytes after incubation in a simple cotton fiber column (Kay and Kayberle, 1972). Trypan blue exclusion of cells indicates 94 to 100% viability. Greater than 10^6 lymphocytes/ml whole blood are obtained by combination of the cotton fiber and isopycnic focusing, resulting in suspensions of 92 to 94% pure lymphocytes. Exclusion of Trypan blue indicates 97 to 100% viability (Kay et al., 1976).

Because of the lack of significant improvement over the cotton fiber method by the combination method; and due to the speed, simplicity, and minimal equipment requirements of the cotton fiber column; and the öbviation of the exposure of the cells to the high centrifugal forces inherent in isopycnic focusing; the method of Kay and Kaeberle (1972) should come into widespread use and, ultimately, become the method of choice for isolating pure, viable samples of peripheral lymphocyte tissue.

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APPENDIX B

MITOCHONDRIAL HETEROGENEITY*

Background

The purity, homogeneity, and functional integrity of the "mitochondrial" fraction obtained by differential centrifugation of single tissue homogenates has been a matter of discussion since the introduction of the subcellular fractionation procedure by Bensley and Hoer (1934). In order to avoid contamination by smaller particulates occurring in the homogenates, at that time collectively referred to as microsomes, elaborate fractionation schedules were devised (Novikoff, et al., 1953). Some degree of heterogeneity within the mitochondrial fraction was initially reported by Kuff and Schneider in 1957 with respect to succinate dehydrogenase. Werkheiser and Bartley (1957) separated the mitochondrial fraction into "heavy, light, and fluffy" subfractions by means of differential centrifugation through 0.25 M sucrose. The heavy subfraction was found to contain twice the sarosine dehydrogenase activity of the light subfraction (Frisell, et al., 1965). Meanwhile, careful investigations with density gradient centrifugation (Beaufey, et al., 1964)

^{*}Taken from an oral research proposition, University of Houston, 1979 by Charles E. Willis.

revealed the presence of two other biological particles, the lysosomes and peroxisomes, in the "mitochondrial" fraction, as well as fragments of the plasma membrane and endoplasmic reticulum (microsomes). Even when corrections were applied to account for the effects of this contamination, differences in biochemical behavior were noted in rat liver mitochondrial subfractions under normal and regenerating conditions (Gear, 1965a,b). Heterogeneity was also observed in yeast mitochondria (Matile and Bahr, 1968). The short (18.5 days) biological half-life observed for mitochondria when compared to the life of the cell (Fletcher and Sanadi, 1961; Beattie, et al., 1967) led some investigators to expect variation in the mitochondrial population within a tissue with respect to age and biochemical composition, while others (de Duve, 1967) maintained that any observed heterogeneity was the result of contamination by other organelles and soluble proteins, or differential fragmentation during the isolation procedure. Patterns of protein incorporation among the subfractions suggested that the light mitochondria might be incomplete, immature organelles; the heavy mitochondria normal; and the fluffy population a combination of regenerating and degenerating mitochondria (Katyare, et al., 1970). More recently, similarly obtained arbitrary subfractions of insect flight muscle mitochondria were demonstrated to be heterogeneous with

respect to phospholipid turnover (Novak, et al., 1979). Pickett, et al. (1976), isolated light and heavy mitochondria on a continuous Ficoll gradient, and although unable to resolve them into discrete subpopulations, found them to be heterogeneous with respect to capacity for oxidative phosphorylation. Murfitt, et al. (1978), used gradients of Metrizamide to separate upper and lower bands of myocardial mitochondria, and noted differences in morphology and oxidative phosphorylation. Functional differences in the absence of osmotic effects is supported by the work of Thompson, et al. (1974) using H_2O/D_2O gradients. Recently, (Wattiaux-de Coninck, et al., 1977), the validity of any isolation method based on centrifugation has been challenged due to the observation that the hydrostatic pressure generated by centrifugation could cause structural damage to the mitochondrial mem-The extent of this process can be monitored by branes. measurement of the free malate dehydrogenase activity in the supernatant, which is normally low since this enzyme is retained in the matrix of intact mitochondria. The effect of pressure on mitochondria is well known; early studies (Beaufay, et al., 1964) report that mitochondria exhibit a second isopycnic point following exposure to dense sucrose solutions. Recently (Higgins, et al., 1978), heterogeneity in mitochondrial function has been observed between morphologically distinct structures within the

same organ. Since much of work on mitochondrial heterogeneity has been done using homogenates of liver, a notably heterogeneous organ (Jungermann and Sasse, 1978), the question of mitochondrial heterogeneity within a single, homogeneous cell type has not been clearly answered.

An important characteristic of mitochondria is that each individual organelle is a discrete genetic entity (Shatz et al., 1964; Borst and Kroon, 1968, Bogenhagen and Clayton, 1977). By virtue of its closed, circular, supercoiled DNA, the mitochondrion is a potential vector for transmission of genetic variation, reminiscent of the "determinant" theory of August Weismann (p. 10, Fulton and Klein). A multitude of mutants have been catalogued and mapped onto the mitochondrial genomes of several species of higher organisms (Tzagoloff and Macino, 1979). The direct transcription products include ribosomal RNA's and tRNA's (which could account for variation in protein incorporation rates), and mRNA's which code for cytochrome oxidase subunits, Cytochrome b and subunits of the reversible ATPase complex (a defect in any one of which might also lead to alterations in the stochiometry of oxidative phosphorylation) (Schatz and Mason, 1974; Mitchell, 1979). Mitochondria are also important structures for the translation of nuclear messenger RNA's (Kisselev, et al., 1975), not only for

some of their own functional components, but also for use by the entire cell (Irwin, et al., 1978). Elaborate coordination schemes have been devised to explain the interaction between nuclear and mitochondrial genes (Freedman and Chan, 1978). Though melting and renaturation studies indicate little or no heterogeneity in mtDNA from green alga (Ryan, et al., 1978), heterogeneity of mtDNA from higher organisms has been observed with regard to primary structure, quarternary structure (see below) and general physical characteristics. MtDNA from various species has been found to differ in buoyant density (Strassberg, et al., 1974), base composition, pyrimidine clustering, and occurrence of "odd" bases (Vanyushin and Kirnos, 1977). A unique mtDNA was found to occur in the sterile "S" cytoplasm of maize by electron microscopy and electrophoresis in agarose gels (Pring, et al., 1977), and later the diversity of mtDNA's from normal maize cytoplasms was established (Levings and Pring, 1977) by means of restriction endonuclease digests. Synenki, et al. (1978) have reported the occurrence of multiple discrete size classes of mtDNA from soybean. MtDNA is known to exist in several forms with regard to "quaternary" structure. These forms include catenated (interlocked) dimers (Hudson and Vinograd, 1967; Clayton and Vinograd, 1967), circular dimers (associated with abnormal cellular states such as cancer; Smith and Vinograd, 1973), as well as monomeric

and replicative forms (Kasumatsu, et al., 1971). Relative occurrence of these forms has been found to vary between tissues and with aging (Piko and Matsumoto, 1977; Piko and Meyer, 1978), and between normal and malignant tissues (Clayton, et al., 1968; Clayton and Vinograd, 1969). Gillum and Clayton (1978) reported that the displacement loop initiation sequence (7.5 S mtDNA) of the replicative form exists as a family of discrete lengths. One proposed mechanism for this phenomenon is that the parental duplex molecules are heterogeneous in the D-loop region. The most straightforward means of detecting heterogenity in the primary structure of mtDNA is through the use of restriction endonuclease digests. In this way, microheterogeneity has been detected in the circular dimer form as compared to the monomeric and catenated forms of mouse LD (cultured cells) and human cells, (Robberson, et al., 1977). Two types of mtDNA were found within a single strain of rat, though no individual rats were found to possess both types. Other rat strains exhibited either one or the other type mtDNA (Hayashi, et al., 1978a; Kroon, et al., 1978; Buzzo, et al., 1978). The restriction pattern trait shows strict maternal inheritance (Hayashi, et al., 1978b), and the results were confirmed for natural populations (Avise, et al., 1979). Maki and Cummings (1977) demonstrated the power of the restriction digest technique when they used mtDNA's to distinguish

between interspecies hybrids of Paramecium aurelia. Though Ascites tumor cell mtDNA's were shown to differ from normal host cell mtDNA's (Hayashi, et al., 1978c), Potter, et al. (1975) detected no difference from different organs of the same individual domestic farm animal. Highlighting the controversy, recently Coote, et al., (1979) demonstrated heterogeneity between mtDNA's of different tissues from the same individual animal. The question remains whether the preparations of mtDNA used as substrate for the restriction digests are single molecular clones or represent mixtures of different molecules. The usual way of resolving the question is to sum up the lengths of the fragments, as determined by comparison with the migration of "known" fragments, and see if it approximates the length of the intact molecule. Even though the sum of the major fragments may approximate the intact length, there exist certain "minor" bands which are difficult to locate and may represent heterogeneity within single preparations of mtDNA. Though the stochiometry of the bands can be determined with some difficulty, accurate methods of quantitation (Pulleyblank, et al., 1977; Willis and Gray, unpublished) are not in general use, so that the relative molar ratios of the bands, which should be one-to-one for a homogeneous molecule, completely digested where all bands are resolved, is usually not measured.

If there are indeed discrete subclasses of different-sized mitochondria, it may be possible to separate them, either analytically or preparatively, by electrophoresis. The electrophoretic mobility of mitochondria was first measured by means of free boundary electrophoresis using a modified Tiselius apparatus (Thompson and McLees, 1961). Evidence showed that the net negative charge borne by the mitochondria was due to membrane binding of $HPO_4^{\overline{-}}$ Electrophoretic mobilities of mitochondria were measured under a variety of conditions of pH and toxicity, and isoelectric pH's were measured (Plummer, 1965) using themicroelectrophoretic apparatus of Gittens and James (1960). Another microelectrophoretic apparatus (Bangham, et al., 1958) was used to compare the properties of heavy, light, and "fluffy" mitochondrial fractions under normal (Katyare, et al., 1970) and abnormal (Koppikar, et al., 1972) conditions. These efforts were largely unsuccessful in detecting significant heterogeneity, probably because of the short path length for observation (too small for marginal differences to be manifested) and because of the arbitrary nature of the fractionations by differential centrifugation (which allows cross-contamination which distorts the averaging of observations in these microdeterminations). Modified zonal electrophoresis on paper was effective in demonstrating the effect of incouplers on mitochondrial properties,

but lacked the resolution necessary to quantify the results (Valdivia, et al., 1973). Continuous flow electrophoresis (Bier, 1957) has been used preparatively to fractionate crude subcellular homogenates (Hannig, 1964a,b; 1967), and was successful in separating mitochondria from microsomes, nuclei, and chloroplasts, but lacked the resolution necessary to detect heterogeneity in mitochondrial population. Under optimal conditions, continuous flow electrophoresis has demonstrated a degree of mitochondrial heterogeneity (Ryan, et al., 1971). A simpler method which holds more promise for the resolution of mitochondrial subclasses is zonal density gradient electrophoresis (Svensson and Valmet, 1955; Brakke, et al., 1968). The use of this method has been restricted to the visual determination of electrophoretic mobility of mitochondria already partially purified by discontinuous density gradient electrophoresis (Vos, et al., 1968). Preliminary results with continuous linear gradients indicate that all of the mitochondrial subfractions obtained by differential centrifugation contain heterogeneously migrating populations of mitochondria.

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APPENDIX C

FORTRAN LISTING OF EXESWL AND ADJUNCT SUBROUTINES

Direct computer printouts for EXESWL, the executive program; SWELL, the error subroutine; and MNWD4A, the search subroutine, are reproduced in their entirity in this section.

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THE OVERALL FRROP OF THE PROSPECTIVE "ODEL IS CALCULATED INCLUMING PLACED STORED E_{M} = THE MARK OF THE STARLE VIELATE INTURATED THE SOLUTION COST THELUDE DECLAPATIONS OF COMMON BLOCK INFO MINUTES ビルト IF(ESS(J) *LT*(SEE(J)+*J5))PEN=PEN+BIG*(ESS(J)-*^SEE(J))**2 [t (SEE (]) * 01 * (ESS (]) - * J2)) b <u>e</u>d=b td+u1 0* (<u>e</u> SS(]) - * U2- SEE (])) * * 3 = NAME OF THE ARRAY INTO WHICH THE CALLING PROGRAM HAS X= NAME OF THE ARRAY IN THICH THE SOUTHFLOW POINT IS IN AC COST= THE NAME OF THE SUBROUTIVE SUBPROSPAN THAT COMPUTES THE VEXT TWO CAPAS ARE APPROVATE FOR MATA W/TIME IN <u> SURROUTI''E MNMD4A(MJCDSTJX, EUJXI''' XUXJVC, UIT'', MNDA)</u> N= ORDEP OF THE PEPAMETER SPACE TO RE SEARCHED OVER IF(ESS(])。GT。10。7)PEW=PEW+RTG+(10。D-ESS(J))++? IF (CAY(J)。GT。10。3)PEN=PEN+4IS+ (CAY(J)-10。Λ)++2 If(CAY(J) LT...(1) PEN=PEN+GIG*(CAY(J)-...) +*? If(TNS_LT_1_00)PEN = PEN + 3IG+(1_0^-T4S)++2 $z + x = 10^{\circ} - 10^{\circ} + 10^{\circ} = 10^{\circ} - 10^{\circ} + 10$ t F (TOTAL_LT_1_00) PFN=PFN+9 TG+(1_7)-TOTAL)++2 F(TOTAL.GT.1.00)PEN=PEN+BIG+(1.00-TOTAL)++2 LF(P(1) *GT** 005) DFN=DFV+RTG*(* 005-P(1))+*? AN INITIAL ESTIMATE FOR THE SOLUTION. DIMENSION X(1) TNS== (ESS(J))/((ESS(J))-(SFE(J))) CONSTPATNTS IF(CAY(K) . LT. D)CAY(K)=0 COST FUNCTION. IS TO NE STADED CONFORMITY TO COST = COST + PENTOTAL = TOTAL + P(K) 00 350 K=1,LL UC = U = SNLRETURN NIX E Z J C U 7 350 C ပပ

EVALUATIONS IN COST. × WORLING SPACE = NAME OF AN ASPAY WITH AT LEAST M+ (N+3) NI EVALUATTONS, BUT HOULD ALLOW A MAX OF 20 FVALUATIONS (TWO LEAST SIGNIFICANT DIGITS = NUMMER OF FUNCTION ς τωτάι ναιυρ = τοται πυηθέα σε εμντιών εναιθατιώνs THUS NEW=1020 WOULD ALLOW A TOTAL OF 1020 FUNCTION NX= NUMBER OF SIGNIFICAMT DIGITS NEEDED FOR CONVERGENCE NC= NUMBER OF SIGNIFICAMT DIGITS NEEDFD FOR CONVERGENCE NITM=(A9S NITM = MAX NUMBER OF SFAPCH CYCLES ALLOWED) ALLOWED ON ANY GIVEN PELATIVE "INI'I SEARCH) ALLOYED REFORE AN ARNOR 14 LEEWINATION) DOUGLE PRECISIOND.H.H.M.X.PI.S1.S2.A.7.C.TESTX = 5*N (IF VITM LT ZERO NO PRINT OUT) LOGICAL VEW, OMCE, NORYTE, REFYN, REVRS, "LCV VIMENSION X(N)XIN(N)WU'(N)WU'(N)X NOISNAWIO RELATIVE MINIMUM SEARCH... "DAGS, DSORT, TOLX FAUIVALFNCF (FPSXS, FPSX4) 102 0105 MXFT = (NFM/130)+100 ("TIU") SAAI = EPSXW = SORT(EPSX) ב גיאדו היצר) ב גיאדו DECLAPED SPACE NOPYTE = NIT"LT.ON ΙΕζ ΜΧΕΡ_αΜΕ_αΩΟ) DATA A1.421.51.51 MXFR = "IFI]-IIXFT REFYN = "FALSE. = FALSE. .FALSE. = 0.1**"X = 0.1**AC DATA AL"/. S/ CZ = ZJXW C LNTESED li XIMIIN EPSCW PEVRS EPSC ONCE FPSX H L L H ≡w û 62

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no 1¤6 J=1≠M
nm(J≠M+₹) = 495( X(J) )*FP5XS
                                                                                                                                                            NEW = .TRUE.
IF( IT.GE.HITMAX ) GOTO 9000
                                                                                                                                                                                  If( NFT_GE_MXFT ) GOTO 2011
IT = IT + 01
                                                                                                                                                                                                                                                                                                                                      VM(I_J) = VM(I_{V+X}) + FPSXS
                                                                                                                                                                                                                                                                            Site (2+1/1) Mu =
0°0
                                                                                                                                                                                                         JEC NORYTE ) GOTO 250
                                                                                                                                                                                                                     (10 + 31 )/C = 3N3
                                                                                                                                                                                                                                                                                                               J= N-I+^1
                                                                                                                                                                                                                                                                                                                                                                                 ASSIGN 250 TO KORYT
                                                                                                                                                                                                                                                                                                                                                J = 1,01
                                                         J = 1,N
                                                                                                                                                                                                                                            PEVRS = . NOT. PEVRS
                                                                              (\Gamma) N I X = (c+N C) W Q
                                                                                                    ASSIGN 190 TO IRT
                                                                                                                                                                                                                                                                   J = 1 , 1
                                                                                                                                                                                                                                                       1=1,1
                                                                                                                                                                                                                                                                                                                                                            PM(J_{\mu}^{+}+1) = X(J)
                                                                    (\Gamma) N I X = (\Gamma) X
                                                                                         FPST = 1.63P
                                                                                                                          FM = F(Ω1)
no 106
                                                                                                                                                                                                                                                                                        (2+N*1)w0
                                                                                                                                                                                                                                                                              DM(1,J) =
20 NFR = DD
                                                                                                                GOTO 53
          NFT = DO
                                             Mp1 = 11
                     UU = SN
                                 υ = 11
                                                        00100
                                                                                                                                                                                                                                CC = SN
                                                                                                                                                                                                                                                                                                                                                U12 U0
                                                                                                                                                                                                                                                       L22 00
                                                                                                                                                                                                                                                                 00 215
                                                                                                                                                                                                                                                                                                     1=[
                                                                               100
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195
196
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210
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220
240
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IF( FOST-FM.LF.FOSCW*( AAS( FM )+FOSCW ) 30TO 80CO
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              TXT = ARS( D<sup>4</sup>(J_R)) / ( ARS( X(J)) + FPSX<sup>4</sup>)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              IF( AXT.LE.EPSXW ) GOTO ROOM
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               ( ( AXA )TASSIIXA )SAA
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            403
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       DM( ] . ] . * n 4( ] . 4)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    Later (1 * Later J * 
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           IFC TXT.LE.AXT ) GOTO 310
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   OM(J_RR) = X(J) - ON(J_RR)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 AXP.LE.AMX ) GOTO
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             ASSIGN 470 TO KP1000
                                                                                                                                                                                            ASSIGN 310 TO VAIDIA
                                                                                                                                                                                                                                                                                                                                         1F( RLE* ) GOTO 1000
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                J=1 ~ N
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             I=1,N
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      J=1 ~N
                                                                                                                                                                                                                                                                                               RLFN = R.LF.N
                                                                                               TOLX = EPSXW
                                                                                                                                               TOLC = FPSCW
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          + 1%A
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          + uXv
                                                                                                                                                                                                                                                                                                                                                                                         TOL X = EDSX
                                                                                                                                                                                                                                                                                                                                                                                                                                            = FPSC
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             5 C 7
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          203
                                                                                                                                                                                                                                            R = R + 01
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   FPST = FM
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             GOTO 1000
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          -
0
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                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      AXT = TXT
60T0 9005
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      CONTINUE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            AXT = D.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             AMX=D.O
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         00 310
                                               CC # 4
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                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          IFC
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                AXP
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                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             AXA
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                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                AXI
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                                                     250
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145
                                                                          = T1LX
                                    NEW = A9S( TXT+AXT ) "LE. E0SXW
                                                                                                                                                                     TF("F(?).LF.F(1) ) GOTO 1201
                                                                         IF( ARS( AL ).LT. TOLX ) AL
H = AL
                           DM(J_I) = DM(J_I)
                                                                                                                                                                                                                                      ASSIGN 1400 TO 19T
          N ~ XW I = I
                                                                                                                                           ASSIGN 1100 TO LAT
                                                                                                                                                    ASSIGN 53 TO JUMP
                  J=1_N
                                                                                                                                                                                                                                                                                                      D0 1500 [=1.M
PI = F(I)
                                                                                                                                                                                                                     H+**JL = XWH
                                                                                           F(1) = F^{N}
                                                                                                                                                                                       GOTO 13PJ
                                                                                                     D(1) = 0.
                                                                                                                                                                                                   H + H = H
                                                                                                                                                                                                                              h = (1) A
                                                                                                               н
Н
                                               G0T0 210
                                                                 AL = ALW
                                                       NFR ≡ Ω∩
CONTINUE
                                                                                                                                                            GOTO 50
                                                                                                                                                                                                                                                 60T0 SU
                                                                                                                                 MP1 = 2
         00 410
00 410
                                                                                                                                                                                H = H
                                                                                                                                                                                                                                                                                               -
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1
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2
                                                                                                                                                                                                           MP1 =
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ب
                                                                                                                                                                                                                                                                   Mp1
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C
                                                                                                                                                                                                                                                                             1500 A =
                                                                                                                                                                                                  1200
                                                                                                                                                                                                                                        1350
                                                                                                                                                                                                                                                          1400
 403
                                                                                                                                                                       1100
                             410
                                                         1000
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TF( (D(MD1)-D(W)-HWX)+HWX *LE* D* ) G)TO 301D
                                                                                                                                                                                                                                                                                                                                 If( DABS( D(1)-D(MP1) ).LF.TESTY ) GOTO 4.000
                                                                                                                                                                                                                                                                                                                                            IF( ABS( F(1)-F(WP1)).GT.TESTC) 60T0 3030
                                                                                                                                                                                                                                                                             TESTX = TOLX*( DABS( D(MP1) ) +TOLX )
TESTC = TOLC*( ABS( F(MP1) )+TOLC )
                                                                                                                                                                                                                                                                                                                                                                                                                                   50 00 51 J=1.N
51 x(J) = 04(J.N+2) + 0M(J.P.P)*D(4P1)
                                                                                                                                                                                                = ( 8+ DSORT( D(5) ) /A
                                                                                                                                                                       IF( D(5).GE.D. ) GOTO 1760
                                                                                                                                                                                                                                                                                                                                                                                      JF( A.NE.D. ) GOTO 1750
            IF( 4.EQ.4 ) GOTO 1500
                                                                                                                                                                                                                            D(HP1) = D(M) + H^{MX}
                                                                                                                                                                                                                                                                                                                                                                                                                                                         (UCU7 25) CON 11 0205
                                                                                                                                                                                                                                                     ASSIGN TOTO TO LET
                                                                                                                                                             0(5) = B+B = A+C
                                                                  h(4P1) = 0.5 + B/b
                                                                                                                                                                                                                                        XmH + XLH = XmH
                                                                                                                                                                                                                                                                                                                                                                                                                                 J = 1 ~ N
                                                                                                                                                                                                                                                                                                                       W'L=I ULLE UU
                                                                                                                                                                                                                                                                                                                                                                                                                   60T0 2041
                                                                                                                                                                                      ρ(5) = Π.
                                                                             GOTO JOAN
                                                    G0T0 1507
                                                                                                                                   GOTO 1652
G0T0 1351
                                                                                                                                                                                                                                                                                                                                                               1 = ]+01
                                                                                                                                                                                                                                                                                                                                                                            CONTINUS
                                                                                                                                                A = 7. + A
                                                                                                                                                                                                                                                                                                                                                                                                                               51
                                                                                                                                                                                                                                                                     GOTO SO
                                         MP1 = 5
                                                                                                         E I N
                                                                                                                       ر
۳
                          3 = U
                                                                                                                                                                                                     n (5)
                                                                                                                                                                                                     1760
3000
                                                                                                                                                                                                                                                                                                                                                                               3030
                                                                                                                                                                                                                                                                                  3020
                                                                                                                                                                                                                                                        3010
              2040
                            2041
                                                                   1900
                                                                                             1700
                                                                                                                                                  1750
```

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IF( F(I).GE.F(4P1) ) GOTO 4727
                             JF( VFR_GT_MXFR ) GOTO 4003
GOTO IRT_(1100,1400,3720,190)
                                                                                                                         IF( \P1_FQ_M+Q1 ) GOTO 4020
ASSIGV 4720 TO JUMP
                                                                                                                                                                                                                                                                                                                                                                                                                                             \widehat{}
                                                                                                                                                                                                                                                                                                                                                                                                                                                           \widehat{}
                                                                                                                                                                                                                                                                                                                                                                                                                                            MXSu3 + XSu3 ) IUUS = MXSd3
                                                                                                                                                                                                                                                                                                                                                                                                                                                            EPSCV = SQRT( FPSC+EPSCV
                                                                                                                                                                                                    ( JV ) STAT + A2+A3S( AL )
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          JF( REFYN ) GATO ODA
53 CALL COST( F(MP1),X )
                                                                                                                                                                                                                                                                                   TXT*(9%L)mA
                                                                                                                                                                                                                                                                                                                                                                               60T0 KB1300, (300, 400)
                                                                                                                                                                                                                                                                                                                                                                                            IFC DACE ) GOTO ROSO
                                                                                                                                                                                                                    IF( RLEN ) GOTO 4015
                                                                                                                                                                                                                                                                                                   IF( RLFN ) GOTO 4035
PO 4932 J=124
                                                                                                                                                                                                                                                                   (()X =
                                             52 6010 IRT (1100-1
4000 50 4010 I=1."
                                                                                                                                                                                                                                                                                                                                                             4035 MET = MET + NFP
                                                                                                                                                                                                                                                     J=1 _N
                                                                                                                                                                                                                                                                                                                                                                                                                             PEFYN = "FALSE.
               NFR = NFR + 0.1
                                                                                                                                                                                                                                     TXT = 1.0 + AL
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        PEEV4 = TPUE.
                                                                                                                                                                                                                                                                                                                                                                                                             ONCE = TRUE
                                                                                                                                                                                                                                                                                                                                               NS = NS + 01
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        FPSYA = CPSV
                                                                                                                                                                       AL = n(MP1)
                                                                                                                                                                                       FM = F(MD1)
                                                                                                                                                                                                                                                                                   DM(J,R) =
                                                                                                                                                                                                                                                                    C444 () WU
                                                                                                                                                                                                                                                                                                                                 (2+1;"[)WU
                                                                                                                                                                                                                                                                                                                                                                                                                                                                          60T0 200
                                                                                                           CONTINUE
                                                                                                                                                         GOT0 50
                                                                                                                                                                                                                                                   02 4 3 0 4
                                                                                           MP1 = 1
                                                                                                                                                                                                                                                                                                                 C214 01
                                                                                                                                                                                                                                                                                                                                 4032
                                                                                                                                                                        4020
                                                                                                                                                                                                                                                                                                                                                                                               A D C O A
                                                                                                           4010
                                                                                                                                                                                                                                                     4015
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            8 0 S 0
                                                                                                                                                                                                                                                                                   403n
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50.90 52.90 50.25 4.0 52.70 8.0 1 FORMAT(11HOMNWD4A, ITI3,4H, VFI6,5H, FUV1PE12,4/17HOPARAMETER VECT 2.0 49.00 2.5 40.00 3.0 49.75 3.5 6.0 52.00 6.5 52.25 7.0 52.50 7.5 10.0 53.3 10.5 53.4 11.0 53.4 2 FORWAT(17HOSEARCH COMPLETED) 51.80 53.20 IF (NORYTE) GOTO 9010 WRITE(6.1) IT.MET.FM.X GOTO KRRYT, (250,9010) TYAEN OT ALCO NEISEA 5.5 5.6 1.5 43.00 1.0 45.00 1 51.20 5.0 51.50 5 53.00 9.0 53.10 9 80R/(9E15.6)) FPSCW = EPSC WRITE(6.2) Ę GOTO 175 0°4100 0°4200 9010 RETURN 22 END 0006 5006 4 8.5 4.5 0-5

Charles Edward Willis, son of Mrs. Charlotte C. Willis and the late Noble S. Willis, was born in Shreveport, Louisiana on November 7, 1953. He graduated from C. E. Byrd High School in May 1971. He graduated from Louisiana State University in Baton Rouge in May, 1975, with a Bachelor of Science degree in General Studies, which included coursework from the United States Air Force Academy and LSU in Shreveport. Upon graduation, he was commissioned in the United States Army Reserve. He married Miss Diana Natalie Gray, also of Shreveport, on June 7, 1975. Their son, Michael, was born May 11, 1976. Charles Willis began graduate study in Nuclear Engineering at Louisiana State University in August, 1975. In addition to being a candidate for the degree of Master of Science in the Department of Nuclear Engineering, he is also a candidate for the Doctorate in Biophysical Sciences at the University of Houston, where he has studied since August, 1977. He is presently employed by Bristol Baylor Laboratories at Baylor College of Medicine in Houston, Texas.

VITA